

July 14, 2008

Beth Ericksen
Engineer
Utah Division of Oil Gas & Mining
1594 West North Temple Street
Salt Lake City, Utah 84114

Dear Ms. Ericksen,

EarthFax

EarthFax
Engineering, Inc.
Engineers/Scientists
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Enclosed is one copy of the second draft of the Notice of Intention to Revise Large Mining Operations for the Ash Grove Cement Company's Hank Allen Pit (Leamington Plant) M/023/004. This submittal includes a replacement copy of the text of the NOI, and replacement copies of the tables and plates requiring edits as noted in your comments for the first draft (submitted March 5, 2007). In addition, addenda have been provided for Appendix 13 of the NOI. Edits have been made in redline/strikeout format. The revisions made in response to the comments on the first draft have been highlighted. Plates, figures, tables, and appendices submitted as revisions for the first draft that did not require additional changes are not being submitted with this draft.

Please let me know if there is anything else that you need, or have any questions. I can be reached at (801) 561-1555, or at amenitove@earthfax.com.

Regards,

Ari Menitove

Geological Engineer

EarthFax Engineering, Inc.

Encl:

NOI text, tables, plates, addenda to Appendix 13

cc: Josh Nelson

RECEIVED
JUL 2 1 2008

DIV. OF OIL, GAS & MINING

Application for Mineral Mine Plan Revision or Amendment

Operator: Ash Grove Cement Company Mine Name: File Number: M/023/004

Provide a detailed listing of all changes to the mining and reclamation plan that will be required as a result of this change. Individually list all maps and drawings that are to be added, replaced, or removed from the plan. Include changes of the table of contents, section of the plan, pages, or other information as needed to specifically locate, identify and revise or amend the existing Mining and Reclamation Plan. Include page, section and drawing numbers as part of the description.

DETAIL	LED SCHEDUL	E OF CHANG	GES TO THE MINING AND RECLAMATION PLAN	
			DESCRIPTION OF MAP, TEXT, OR MATERIALS TO BE CHANGED	
x ADD	□ REPLACE	☐ REMOVE	Table of Contents. Added entry for new section 110.6.	
x ADD	□ REPLACE	□ REMOVE	p. vi – vii. Updated list of changes.	
x ADD	□ REPLACE	C REMOVE	p. vii. Added language indicating that the pit design complies with the highwall stability evaluation recommendations.	
x ADD	□ REPLACE	D REMOVE	p. 105-3, §105.3.14. Added text to say that limestone highwalls we be sloped at a maximum angle of 2V:1H. Revised list of pit floor areas not to be revegetated.	
x ADD	× REPLACE	□ REMOVE	p. 106-1, 106-2, §106.2. Added a statement addressing the issue of deleterious materials. Also updated the description of the Mine Plan Summary.	
x ADD	x REPLACE	□ REMOVE	p. 106-3, §106.3. Updated life-of-mine estimate. Clarified description of disturbance acreages.	
x ADD	x REPLACE	□ REMOVE	p. 106-20, §106.4. Updated life-of-mine estimate. Added annual limestone and wasterock production amounts. Also added annual topsoil recovery amounts.	
□ ADD	x REPLACE	[] REMOVE	p.106-21. Table 4-106.4-1. Replaced table with updated values.	
× ADD	□ REPLACE	□ REMOVE	p. 106-24, §106.6. Clarified statement about topsoil handling.	
□ ADD	× REPLACE	☐ REMOVE	p. 106-27, §106.8. Updated water elevation in water well.	
× ADD	☐ REPLACE	C REMOVE	p. 106-27 §106.9. Added text to describe the dimensions and volume of the waste stockpile. Also provided drainage control information.	
× ADD	x REPLACE	□ REMOVE	p. 107-1,2, \$107.1.12. Updated waste disposal service providers. Added text to describe handling and disposal of deleterious materials.	
x ADD	[] REPLACE	□ REMOVE	p. 107-2, §107.1.14. Added text to describe the placement of highwall warning signs.	
x ADD	☐ REPLACE	☐ REMOVE	p. 107-3, §107.2. Added text to describe Pond #7.	
x ADD	☐ REPLACE	□ REMOVE	p. 107-3, §107.4. Added text to describe handling, storage, and disposal of hazardous materials.	
× ADD	☐ REPLACE	□ REMOVE	p. 109-3, §109.3. Revised statement addressing topsoil storage.	
× ADD	□ REPLACE	□ REMOVE	p. 109-3, §109.4. Revised description of highwall design. Provided Utah DAQ Title V Operating Permit number.	
× ADD	□ REPLACE	□ REMOVE	p. 110-1, 110-2, §110.2. Updated the description of the manner and extent of reclamation. Added text to reiterate maximum highwall slope angles. Added text to explain runoff and erosion control at the waste rock storage pile. Also added volume of waste rock and storage information for the Southwest Pit as requested.	
□ ADD	☐ REPLACE	x REMOVE	p. 110-3, §110.2. Removed Table 4-110-2-1	
□ ADD	☐ REPLACE	x REMOVE	p. 110-4, §110.2. Removed Table 4-110-2-2	
x ADD	□ REPLACE	E) REMOVE	p. 110-5, §110.5.11. Added text that stated pit floors would not be revegetated, which is consistent with what was originally stated in §105.3.14.	
x ADD	□ REPLACE	□ REMOVE	p. 110-11, §110.6. Added this section as requested.	

Revision Table

x ADD	• REPLACE	• REMOVE	p. 111-1, \$111.1.12. Added language to assure that wastes would be disposed of using environmentally protective ways.
x ADD	• REPLACE	• REMOVE	p. 111-1, §111.1.14. Added language to describe signage during reclamation.
× ADD	• REPLACE	• REMOVE	p. 111-2, §111.1.15. Added elaborative text as requested.
× ADD	• REPLACE	• REMOVE	p. 111-4, §111.4. Added language to indicate that any deleterious materials encountered during reclamation will be disposed of as specified in §107.1.12.
CIDA CI	× REPLACE	• REMOVE	p. 111-4, §111.6. No response to specific comments required. DOGM comments appear to refer to rock slope stability whereas this section addresses soil slope stability. The stability of the only soil slope at the mine (the waste rock pile) is adequately discussed in this section. Note that slope angle of the topsoil stockpile has been changed.
□ ADD	* REPLACE	• REMOVE	p. 112-1 to 112-3, §112.1. Updated variance requests.
× ADD	× REPLACE	• REMOVE	p. 113-1, 113-2, §113.3. Added text to explain that the surety estimate is based on both RSMeans costs and site-specific estimates. Also revised description of surety estimate.
× ADD	• REPLACE	• REMOVE	§113.3. Added Table 113-3-1 (Surety Summary). Added Mob/Demob Costs for Reclamation Equipment Table to calculate mob/demob costs.
× ADD	• REPLACE	• REMOVE	Appendix 2. Drawing R647-4-105.1Ba. Added June 2006 quarry disturbance boundary.
□ ADD	× REPLACE	• REMOVE	Appendix 5. Drawing R647-4-105.2Q. Added notation describing that the Chaffin Quarries are Pre-SMCRA.
D ADD	* REPLACE	- REMOVE	Appendix 8. Drawing R647-4-105.3.17. Updated acreages in legend and for waste rock stockpile. Also added locations of reclamation channels.
ממג 🗅	× REPLACE	• REMOVE	Appendix 8A. Drawing R647-4-108. Added locations of borings described in the 2001 Seegmiller report.
□ ADD	× REPLACE	• REMOVE	Appendix 9. Drawing R647-4-109. Updated acreage of waste rock stockpile.
× ADD	× REPLACE	• REMOVE	Appendix 13. Updated hydrology calculations for the reclamation drainage channels. Added hydrology calculations for Pond 7.

I hereby certify that I am a responsible official of the applicant and that the information contained in this application is true and correct to the best of my information and belief in all respects with the laws of Utah in reference to commitments and obligations, herein.

July 8, 2008 Date Bruce Newell

Plant Manager

Leamington Plant, Ash Grove Cement

Company

	FOR	DOGM	USE ONLY:
F	ile#:		1
Approved	i::		
Bond Adjustment: from (\$	1		
to \$			

Return to: State of Utah Department of Natural Resources Division of Oil, Gas and Mining 1594 West North Temple, Suite 1210 Box 145801 Salt Lake City, Utah 84114-5801 Phone: (801) 538-5291 Fax: (801) 359-3940

O:\FORMS\MR-REV-att.doc Instructions - Amend or Revise Mining Plan Page 3 of 3

NOTICE OF INTENTION TO REVISE LARGE MINING OPERATIONS LEAMINGTON PLANT AND QUARRY

PERMIT NO. M/023/004

Revised Text/Tables

Submitted To:

DIVISION OF OIL, GAS, AND MINING
SALT LAKE CITY, UTAH

By:

ASH GROVE CEMENT COMPANY LEAMINGTON PLANT P. O. BOX 51 NEPHI, UTAH 84648

Submittal Date: June 27, 2000
Revised and Re-submitted February 28, 2001
Revised and Re-submitted August 31, 2001
Revised and Re-submitted March 5, 2007
Revised and Re-submitted July 14, 2008

NOTICE OF INTENTION TO REVISE MINING OPERATIONS

ASH GROVE CEMENT COMPANY LEAMINGTON PLANT and QUARRY JUAB AND MILLARD COUNTIES, UTAH PERMIT NO. M/023/004

TABLE OF CONTENTS

	yi.
II. Introd	uctionii.
	of Intention to Revise Mining Operations R-REV (REVISED/96)MR-1
Progra	ses to UTDOGM Minerals Reclamation m Rules (Last Revised 1994): -LARGE MINING OPERATIONS
R647-4-104 . 104.1 N	Operator(s), Surface and Mineral Owner(s). ame of operator responsible104-1
104.2 N	ame of surface landowner(s)104-1
104.3 F	ederal mining claim numbers, etc104-2
R647-4-105. 105.1.11 105.1.12 105.1.13 105.1.14 105.2 105.2.11 105.2.12	Maps, Drawings and Photographs. Topographic base map
105.3.11 105.3.12 105.3.13 105.3.14 105.3.15 105.3.16 105.3.17 105.3.18	Regraded slopes steeper than 2h:1v

105.4	Photographs of the site to show existing vegetation and surface conditions	105-8
R647-4-106	Operation Plan.	
106.1 T	Type of mineral(s) to be mined	106-1
106.2 T	Types of operations to be conducted	106-1
	stimated acreages proposed to be disturbed and/or reclaimed annually or sequentially	106-3
106.4 N	ature of materials to be mined	106-20
106.5 E	xisting soil types	106-20
	lan for protecting and re-depositing existing soils	
106.7 E	xisting vegetative communities	106-24
106.8 D	epth to groundwater	106-26
	roposed location and size of ore and waste stockpiles, tailings facilities and water storage/treatment ponds	106-27
R647-4-107. 107.1.11 107.1.12 107.1.13 107.1.14 107.1.15 107.2 107.3 107.4	Public safety and welfare	107-1 107-2 107-2 107-2 107-3 107-3
107.5	Soils	107-3
107.6	Concurrent reclamation	107-8
R647-4-108.	Hole Plugging Requirements.	
	Setting a nonmetallic permapluq	108-1
	Tillable farmland	

	108.2 Drill holes that encounter water108-1
	108.2.11 Artesian flow108-1
	108.2.12 Significant nonartesian flow
	108.2.12.111 50 foot cement plug
	108.2.12.112 Filling from bottom up
	100v2.12v2.2 22121.9 22om 0000m april vivi vivi vivi vivi vivi
RE	547-4-109. Impact Assessment.
211	109.1 Surface and groundwater systems
	109.1 Surface and groundwater systems
	100 0 0 0 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
	109.2 State and federal threatened and endangered
	species109-1
	109.3 Existing soil resources109-2
	109.4 Slope stability, erosion control, air quality109-2
	109.5 Proposed mitigation of impacts109-3
R6	47-4-110. Reclamation Plan.
	110.1 Current land use and proposed postmining land
	use110-1
	110.2 Manner and extent of reclamation110-1
	110.2 Haimer and extent of recramation
	110.3 Surface facilities to be left as part of
	postmining land use110-5
	postmining tand use
	110.4 Treatment, location and disposition of any
	deleterious or acid-forming material110-5
	440 5 77
	110.5 Planting program to re-vegetate disturbed area110-5
	110.5.11 Grading and/or stabilization110-5
	110.5.12 No original protective cover110-11
	110.6 Operator's Statement110-11
R6	47-4-111. Reclamation Practices.
	111.1 Public safety and welfare111-1
	111.1.11 Permanent sealing of shafts and tunnels111-1
	111.1.12 Disposal of trash, scrap metal and wood111-1
	111.1.13 Plugging of drill holes
	111.1.14 Posting of appropriate warning signs111-1
	111.1.15 Construction of berms, fences and/or barriers111-2
	TITILITY CONDUCTOR OF BELLEY TENECOS UNA, OF BUILTOID.
	111.2 Drainages111-2
	TITILE DIGITAGES
	111.3 Erosion Control111-2
	TIT. J DEOSTON CONCLUT
	111.4 Deleterious Materials111-4
	TITE DETECTIONS NUCLEITATS

	111.5	Land Use111-4
	111.6	Slopes111-4
	111.7	Highwalls111-4
	111.8	Roads and Pads111-5
	111.9	Dams and Impoundments111-6
	111.10	Trenches and Pits111-6
	111.11	Structures and Equipment111-6
	111.12	Topsoil Redistribution
n.c	111.13. 111.13.	Re-vegetation
Кb		Request for variance
		1 Rule to which variance is requested112-1
		2 Variance requested and description112-1
		3 Justification for the variance
	112.1.1	4 Alternate methods to be utilized112-3
	112.2 V	ariance shall be granted if consistent with Act112-3
	112.3 A	pproval of variance by Division in writing112-4
R6	47-4-113	S. Surety.
		roviding reclamation surety to Division113-1
	113.2 D	ivision will not require separate surety113-1
		ivision shall determine the required surety mount
		eclamation Contract (FORM MR-RC)113-2
		1. Corporate surety bond113-2
		2. Federally-insured certificate of deposit113-2
		3. Cash113-2
		4. Irrevocable letter of credit
		5. Escrow accounts
	113.4.10	6. Written self-bonding agreement113-2
	113.5 St	arety shall be required113-3

113.	.6 Adjustments or revisions	.113-3	
v.	List of Figures		
VI.	List of Tables		
VII.	List of Drawings		
VIII.	List of Appendices		

LIST OF FIGURES

Figure	1 Site Vic	cinity Map	iii.
Figure	2 Quarry 1	Location Map	iv.
Figure	4-106.1-1	Stratigraphic Column	106-2
Figure	4-106.9-1	A Geologic Cross-Section A-A' Central Block	.106-46
Figure	4-106.9-1	Geologic Cross-Section B-B' Northeast Block	106-7
Figure	4-106.9-10	Geologic Cross-Section C-C' Southwest Block	106-8
	Figure 4106-15	-106.9-2 Central Pit Bench level 5340	
		-106.9-3 Geologic Cross-Section B-B' No: Block	
	Figure 4	1-106.9-4 Northeast Pit Bench Level	
Figure	4-106.5 Sc	oil Survey Map	.106-22
Figure	4-107.3-1	Straw or Hay Bale Check Dam	.107-4
Figure	4-107.3-2	Rock Check Dam	.107-5
Figure	4-107.3-3	Typical Rock Riprap Drop Structure Profile View	.107-6
Figure		Typical Rock Riprap Drop Structure Cross Section View	.107-7
		LIST OF TABLES	
Section F	8647-4-106		
Table 4	-106.4-1 T	Cotal Schedule Quality Report for the Life of Quarry	.106-21

Section R647-4-110

Table 4	-110		Mixture110-7
Table 4	-110		k Fragmentation Size - Combined nale Results110-3
Table 4	-110		k Fragmentation Size - Combined imestone Results110-4
Section R	647-	4-111	
Table 4	-111	2-1 Re	clamation Channel Summary111-3
Section R	647-	4-113	
Table 4	l-113	3-3-1 SUR	ETY SUMMARY113-4
lastica D	647	4 106 Om	LIST OF DRAWINGS
ection K	04/-	#-Ing Obe	eration Plan
Drawing	No.	4-106-1	63 Million Ton Mine Plan Ultimate Mine Map January 1999106-5
Drawing	No.	4-106-2	REMOVED63 Million Ton Mine Plan January 2000106-6
Drawing	No.	4-106-3	REMOVED63 Million Ton Mine Plan January 2001106-7
Drawing	No.	4-106-4	REMOVED63 Million Ton Mine Plan January 2002106-8
Drawing	No.	4-106-5	REMOVED63 Million Ton Mine Plan January 2003106-9
Drawing	No.	4-106-6	63 REMOVEDMillion Ton Mine Plan January 2004106-10
Drawing	No.	4-106-7	REMOVED63 Million Ton Mine Plan January 2009106-11
Drawing	No.	4-106-8	63 REMOVEDMillion Ton Mine Plan January 2019106-12
Drawing	No.	4-106-9	REMOVED <mark>63 Million Ton Mine Plan</mark> January 2029106-13
	Table 4 Table 4 Table 6 Table 6 Table 6 Table 6 Table 7 Table 8 Table 8 Table 7 Table 9 Table	Table 4-110 Table 4-110 Section R647- Table 4-113 Section R647- Table 4-113 Section R647- Drawing No. Drawing No.	Table 4-110.2-1 Rock Signature Table 4-110.2-2 Rock Line Table 4-110.2-2 Rock Line Table 4-111 Table 4-111-2-1 Resection R647-4-113 Table 4-113-3-1 SUR Table 4-113-3-1 SUR Drawing No. 4-106-1 Drawing No. 4-106-2 Drawing No. 4-106-3 Drawing No. 4-106-4 Drawing No. 4-106-5 Drawing No. 4-106-6 Drawing No. 4-106-7 Drawing No. 4-106-7

Drawing	No.	4-106-10	REMOVED63 Million Ton Mine Plan January 2039106-14
Drawing	No.	4-106-11	REMOVED63 Million Ton Mine Plan September 2049106-17
Drawing	No.	4-106-12	REMOVED63 Million Ton Mine Plan September 2059106-18

LIST OF APPENDICES

- 1. Drawing No. R647-4-104.3L Land Ownership Map
- 2. Drawing No. R647-4-105.1Ba Base Map
- 3. Drawing No. R647-4-105.4 Leamington Plant and Quarry (aerial photograph)
- 4. Drawing No. R647-4-105.2P Surface Facilities Plant
- 5. Drawing No. R647-4-105.2Q Surface Facilities Quarry
- 6. Geology of the Champlin Peak Quadrangle, Juab and Millard Counties, Utah
- 7. Drawing No. 647-4-107.2 Drainage Control
- 8. Drawing No. R647-4-105.3.17 Reclamation Activities & Treatment Proposed Area To Be Reclaimed and Revegetated
- 8A. Drawing No. 647-4.108 Geologic Control
- 9. Drawing No. R647-4-109 Proposed Life-Of-Quarry Disturbance
- 10. Drawing No. R647-4-113 Comparison of Original Bonded Area to Present Disturbance Limit
- 11. Environmental Assessment Input
- 11A. Soil Conservation Service Soil and Vegetation Survey
- 12. Biological Assessment for Threatened, Endangered, and Proposed Species for the proposed Ash Grove Cement Plant Expansion
- 12A. Biological Evaluation for Sensitive Plant and Animal Species for the Proposed Ash Grove Cement Plant Expansion
- 13. Surface Drainage Martin Marietta Cement Plant Leamington,
 Utah
- 14. 1993-94 Annual Report of Findings and Water Withdrawals
- 15. Initial Evaluation, Highwall Slope Stability, Hank Allen Quarry, Ash Grove Cement Company, Juab and Millard Counties, Utah

16. Highwall Stability Evaluation: Ultimate Pit Slope Angles,
Hank Allen Quarry - Leamington Plant, Central and
Northeast Block Pits, Juab and Millard Counties, Utah.

NOTICE OF INTENTION TO REVISE MINING OPERATIONS (May 24March 5July 14, 200780)

ASH GROVE CEMENT COMPANY LEAMINGTON PLANT and QUARRY JUAB AND MILLARD COUNTIES, UTAH PERMIT NO. M/023/004

SUMMARY

Ash Grove Cement Company (the Operator) is pleased to submit this document, entitled "Notice of Intention to Revise Large Mining Operations (Permit No. M/023/004)" (the NOI), for the Leamington Plant to the State of Utah, Department of Natural Resources, Division of Oil, Gas and Mining (the Division), for its review and comment. Ash Grove respectfully requests that the Division grant approval for the revisions to the mining operation described in this submittal.

This NOI is submitted in accordance with the Utah Department of Natural Resources, Division of Oil, Gas and Mining, Minerals Reclamation Program, Rules R647-1 through R647-5, which was last revised in 1994 2006 (the Rules). More specifically, this submittal is made in compliance with the requirements of Section R647-4 Large Mining Operations. This submittal is organized and presented in a format which repeats each section of the Rules followed by Ash Groves' response. The submittal includes narrative text in response to the Rules and figures, tables, drawings and maps as required by the Rules and/or to provide additional information to support the responses.

Ash Grove owns lands, located in Juab and Millard Counties, near the town of Leamington, Utah, on which it operates a surface limestone quarry for the production of limestone and shale. The limestone and shale are used as raw products in the manufacture of Portland cement at the Leamington Plant. This NOI provides information, as required by the Division's Rules, to address proposed changes in the mining plans, mining operations and reclamation by Ash Grove at the Leamington Plant and Quarry.

This NOI describes the proposed revisions to the life-of-quarry mining plan, provides a summary of reclamation operations and includes a revised calculation of the estimated reclamation cost. Additionally, the NOI includes various figures, tables, maps and drawings to further explain the revisions to the mining operations.

INTRODUCTION

Ash Grove Cement Company (the Operator) owns and operates the Leamington Plant (the Plant), located in Juab County, and the adjacent Quarry (the Quarry), located in Juab and Millard Counties, Utah. The Plant and Quarry are located adjacent to Highway 132, five miles northeast of the town of Leamington and approximately 23.5 miles southwest of Nephi, Utah, as shown on the Site Vicinity Map(Figure 1) in this section of the NOI.

The Plant is located in Leamington Canyon, south of and adjacent to the Sevier River. The Plant is located in parts of Sections 32 and 33, Township 14 South and Range 3 West. The Quarry is located south of the Plant in the Canyon Mountains. The present active Quarry operations are located in part of Section 33, Township 14 South and Range 3 West and part of Section 4, Township 15 South and Range 3 West. The combined facilities are located entirely on lands owned in fee by Ash Grove, located in all or part of Sections 32, 33 and 34, Township 14 South and Range 3 West, and Sections 3, 4 and 5, Township 15 South and Range 3 West.

The Plant and Quarry are located on the Champlin Peak, Utah U.S. Geological Survey 7.5' Series topographic map sheet dated 1967, as shown on the Quarry Location Map (Figure 2). The natural ground elevation of the site varies from 4,825 feet above mean sea level in the vicinity of the railroad/truck load-out silos adjacent to the UP Railroad to 6,314 feet near the top bench of the Quarry.

The Quarry is operated by Ash Grove Cement Company and presently produces approximately 975,000900,000 tons of limestone and 14,000129,000 tons of shale annually. The limestone and shale are used by Ash Grove as part of the components of the kiln feed used by the Plant in the manufacture of Portland cement. The cement is transported from the Plant to the consumer by truck and rail.

The Quarry and Plant were originally developed by Martin Marietta Cement Western Division (the original Permittee). Martin Marietta referred to the Quarry as the Hank Allen Quarry in honor of the geologist who identified and explored the limestone deposit. A Notice of Intention to Commence Mining Operations, dated December 1979 (herein referred to as the "original NOI"), was submitted by Martin Marietta and received by the Division on December 15, 1979. The original NOI included a total of 273 acres to be disturbed over an estimated forty years of mining operations. This total disturbance area included: 177 acres for the Quarry, 7 acres for a quartzite quarry (silica source),44 acres for a waste dust area, and 45 acres for the Plant, which was referred to as the "manufacturing area".

FIGURE 1 - SITE VICINITY MAP

FIGURE 2 - QUARRY LOCATION MAP

The original reclamation bond was posted on February 14, 1980, as a surety in the amount of \$386,000. The Division completed its review on February 25, 1980, and prepared an Executive Summary for the Board of Oil, Gas and Mining. After receiving public comment and being provided with acceptable reclamation surety, the Division issued Permit No. M/023/004.

Plant construction and Quarry development began on June 9, 19811980. Commercial operations and the production of cement began in 1983—November 1981 by Martin Marietta. Southwestern Portland Cement operated the Plant under a lease agreement with Martin Marietta between 1984 and 1989. Ash Grove purchased the Leamington Plant and Quarry from Martin Marietta on May 8, 1989. Ash Grove has operated the Plant and Quarry since that time.

After its acquisition of the Plant and Quarry, Ash Grove began a program to plan for growth. Various mining plans were developed and modifications and improvements were made to the Plant and Quarry. Mine planning completed in 1994 resulted in a proposed expansion of the Quarry, use of out-of-pit waste shale placement areas, relocation of the crusher and the decision to replace the truck haulage system with a portable crusher and conveyor haulage system.

Based on this mine plan, Ash Grove submitted a Notice of Intention to Revise Large Mining Operation, dated February 28, 1995 (herein referred to as the "1995 NOI"), to the Division. The Division began its review of the 1995 NOI. During this period Ash Grove continued to examine its mining and haulage plans. This review process showed that the economics of the proposed portable crusher and conveyor system were not acceptable to Ash Grove. It was decided to continue with the truck-loader mining method, but utilize larger, more efficient 100-ton haul trucks.

The Division provided its initial comments on the 1995 NOI to Ash Grove by letter dated June 8, 1995. Ash Grove reviewed the Division's comments and responded by letter, dated January 16, 1996. The Division responded to Ash Grove by letter, dated April 4, 1996, and identified a number of "technical concerns" which needed to be addressed before the Division could proceed to issue tentative approval.

During the review/response process of the 1995 NOI between the Division and Ash Grove, Ash Grove submitted, by letter dated July 8, 1996, a request for variance under Rule 647-4-111.7 Reclamation Practices. This request was for a variance for the final highwall slope for the current operations. The Division granted the variance by letter dated July 23, 1996. This variance allowed Ash Grove "...to construct highwalls which are approximately 63° in the 'current quarry area' as shown on the maps included with the April

4, 1996, letter." Ash Grove continued formulating its response to the Division's April 4, 1996, comments to the 1995 NOI.

After further reviewing the mining reserves and long-range mining plans, Ash Grove requested in November 1998, that the 1995 NOI submittal (which was never formally approved) be withdrawn. Ash Grove would submit a new NOI that would more accurately describe its current and proposed mining operations and long-range mining plans. A revised Base Map was submitted to the Division in November 1998, to serve as an interim measure while completion of the new NOI was in progress. The following sections of this report combine to form the new submittal for the NOI as required by the Division. After responding to additional comments the NOI initially submitted in 1998 was approved in 2001.

This NOI provides new information describing the additional proposed changes in the mining operation, proposed reclamation of disturbed lands, and a new calculation of the estimated costs of reclaiming the Plant and Quarry. Additionally, this submittal includes a revised Reclamation Surety Estimate form based on the calculation of the estimated costs to reclaim the final Plant and Quarry.

Ash Grove requests the Division's approval of this NOI and the revisions to the existing Permit No. M/023/004 which include, but are not limited to, the following changes:

- 1. Revision of the current and proposed disturbance limit and a design for pit expansion in the central block, northeast block, and a new southwest block.
- 2. Revision of the reclamation surety estimate.
- 3. Variance request from Rule R647-4-111.7 to allow construction of limestone highwalls with slopes of 2H:1V (63.4°). The slopes will consist of 60-foot tall bench faces and 30-foot wide benches. The south face of the central pit will have 3 50-foot wide stepout benches, as recommended in a slope stability study performed at the pit.
- 4. The slope stability study mentioned in item 3 has been submitted for inclusion in this NOI.
- 5. Variance request from Rule 647-4-111.8 to allow for two segments of access roads to remain partially unreclaimed after reclamation in order to allow landowner access for the Operator as well as adjacent landowners.

- 6. Submission of design hydrology calculations for Sedimentation Pond #7 and the reclamation drainage channels.
- 1. Revision of the current Permit Boundary to include all lands owned by Ash Grove that are presently proposed for use as industrial/mining in connection with the Leamington Plant and Quarry and for future expansion into the Northeast and Southwest blocks.
- 2. Revision of the current Disturbance Limit Boundary to include additional lands needed for the proposed expansion of the Quarry operation into the Northeast and Southwest blocks.
- 3. Revision of the current reclamation surety to include all lands that have been disturbed to date and are proposed to be disturbed over the life of the Quarry operation.
- 4. Variance request from Rule R647-4-111.7 to allow construction of highwall slopes of 2 vertical to 1 horizontal (approximately 63 degrees) in limestone in any mining area within the Proposed Permit Boundary.
- 5. The quartzite quarry included in the original permit is no longer active. There is not a small portable crusher located at the quartzite quarry.
- 65. Three stratigraphic units, identified as the "L3" limestone, the "S3" shale and the "L4" limestone will be mined in the Central and Southwest Pits. Seven stratigraphic units, identified as the "L1" through "L4" limestones and the "s1" through "s3", shales will be mined in the Northeast pit.instead of the seven units identified in the original permit.
- 10. Construction of settling ponds for waste disposal areas.
- 11. The proposed method and conduct of reclamation operations, including waste rock disposal areas.
- 127. Quarry benches are designed to be 60 feet vertical and 30 feet horizontal, instead of 60 feet vertical and 40 feet horizontal.

INSTRUCTIONS to REVISE or AMEND MINING OPERATIONS NOTICE OF INTENTION

When an operator intends to revise or amend a mining operation, a **notice** to Amend or Revise the mining and reclamation plan **must be submitted** to the Division **and approved prior to creating any disturbance beyond what has already been approved.** The notice must include all information, concerning the revision or amendment, that would have been required if it had been included in the original Notice of Intention (NOI).

"REVISION" means a significant change to the approved Notice of Intention to Conduct Mining Operations, which will increase the amount of land affected or alter the location and type of onsite surface facilities such that the nature of the reclamation plan will differ substantially from the approved Notice of Intention. Revisions require a formal public notice of tentative approval and may require a change in the amount of reclamation surety.

"AMENDMENT" is an insignificant change to the approved Notice of Intention. An amendment requires Division approval, but does not require public notice.

The Division will determine whether a request for change is significant or insignificant on an individual case-by-case basis.

Instructions:

- Changes to the mining and reclamation plan are made by providing a completely new plan or by adding, replacing, or removing pages to the current plan. Detailed instructions for adding or replacing pages and maps must be included (please identify on the attached form MR-REVatt).
- Text changes should be shown in a redline/strikeout format.
- The amended application should be accompanied by a cover letter: referring to the permit number, operator name and mine; describing the contents; and referencing any Division action that initiated the change (i.e. Notice of Violation, previous review, Division Order).
- The submitted revision or amendment must be complete and should not rely on additional materials that will be submitted at a later date.
- Form MR-REV-att, or equivalent, must be submitted with the application for change.

After the Division conditionally approves the change, two clean copies will be requested which will be stamped "approved" and one copy returned for your copy of the mining and reclamation plan. The change is now approved and you may proceed with your plans.

Identify any changes this modification will have to:

I. General Information (R647-4-104)

Location of Proposed Activities:

COUNTY: Juab and Millard Counties

• LEGAL DESCRIPTION: T. 14S, R. 3W, S. 32 NE¼, S. 33 NW¼, SW¼, and SE¼ and S. 34 SWSWSW and T. 15S, R. 3W, S. 3 NW¼ and NWNE, S. 4 N½, N½SE, and N½SW, and S. 5 NESE, SENE

Ownership of Land Surface:

• Private (Fee): Ash Grove Cement Company

• State of Utah (SITLA) lands: NO

• Public Domain BLM): NO

• National Forest (USFS): NO

Ownership of Minerals:

• Private (Fee): Ash Grove Cement Company

• State of Utah (SITLA) lands: NO

• Public Domain BLM): NO

National Forest (USFS): NO

BLM Lease or Project File Number(s): Not Applicable

USFS assigned Project Number(s): Not Applicable

• Utah State Lease Numbers(s): Not Applicable

II. MAPS, DRAWINGS & PHOTOGRAPHS (Rule R647-4-105)

Appropriate maps, drawings, plates, etc. should be provided that are pertinent to the revision, or amendment of mining operations. Please provide a revised map outlining the previously approved and the new proposed disturbed area boundaries. These materials should be prepared according to the requirements of Rule R647-4-105.

A list of the maps, drawings, figures, and aerial photographs is provided in the Table of Contents of this NOI. A list of the following Maps and Figures have been updated:

R647-4-104.3L, R647-4-105.1Ba, R647-4-105.3-17, R647-4-105.4, R647-4-105.2Q, R647-4-106-1, R647-4-106.5, R647-4-106.9-1A, 1B, and 1C, R647-4-107.2, R647-4-108, R647-4-109, and R647-4-113.

III. OPERATION PLAN (Rule R647-4-106)

All appropriate information requirements outlined under Rule R647-4-106 must be addressed in the application. Identify additional proposed surface disturbance. Include the total number of acres to be affected by the revision or amendment.

The mining operation will be conducted as described in the this Notice of Intention to Commence Mining Operations and and approved by the Division. A description of the proposed operation plan with an explanation of the proposed revisions to the mining plan is provided in Section R647-4-106 Operation Plan of this NOI.

IV. IMPACT ASSESSMENT (Rule R647-4-109)

Provide information required under Rule R647-4-109 regarding projected potential surface and/or subsurface impacts that may be associated with the proposed change(s) in mining operations.

The types of impacts associated with the revised mining plan and proposed changes in mining operations are presented in this NOI. These proposed changes include: an expansion of mining operations further into an additional reserve block located northeast of the original central mining block; the expansion of the central pit to the southwest; the possible addition of an out-of-pit waste rock storage area; and disturbance of additional acres which are needed for the proposed expansion of the mining operations. A description of these impacts is provided in Section R647-4-109 Impact Assessment of this NOI.

V. RECLAMATION PLAN (Rule R647-4-110)

Outline any proposed changes to the originally approved reclamation plan. Address all appropriate sections of Rule R647-4-110 as they apply to the proposed change(s) in mining operations.

Reclamation operations will be conducted as described in Section R647-4-110 Reclamation Plan of this NOI.

VI. VARIANCE (Rule R647-4-112)

Identify any requests for variance from the requirements of rules R647-4-107, -108, or -111. A narrative justification and alternate methods or mitigating measures must be included for each variance request.

No new request for variance from the requirements of Rules R647-4-107 or -108 is made in this submittal as previously permitted. A variance to rule R647-4-111.8 Roads and Pads is requested to allow two roads to remain after reclamation. The roads to remain after reclamation will be dirt roads with a nominal width of 12 feet. They will be used for reclamation monitoring and access by landowners. However, the variances previously approved by the Division for a final highwall slope of 2 vertical to 1 horizontal (approximately 66°) on limestone slopes and 1 horizontal to 1 vertical horizontal (approximately 45°) in shale is requested to be approved for the expanded mine areas. A description of the requested variances is provided in Section R647-4-112 of this NOI.

VII. SURETY (Rule 647-4-113)

Reclamation Surety: Indicate whether the proposed activities will change the amount of work required to reclaim the mine site. If significant changes will result, then an itemized reclamation cost estimate should be provided (and attached) with direct reference to the specifics of the proposed change(s). This information will be used to assist the Division in determining any reclamation surety adjustments required for the operation.

The proposed changes in the conduct of mining operations in the Central reserve block, the addition of the southwest pit, and the expansion of the mining operation into the Northeast reserve block, as described in this NOI, will increase the amount of land disturbed. This proposed expansion will result in a change to the amount of work required to reclaim the mine site. Information to adjust the bond calculation is provided in this Application.

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Instructions - Amend or Revise Mining Plan Page 2 of 3 Form MR-REV-att (DOGM - Revise/Amend Change Form) (Revised September 14, 2005)

Application for Mineral Mine Plan Revision or Amendment

Operator: Ash Grove Cement Company

Mine Name: File Number: M/023/004

Provide a detailed listing of all changes to the mining and reclamation plan that will be required as a result of this change. Individually list all maps and drawings that are to be added, replaced, or removed from the plan. Include changes of the table of contents, section of the plan, pages, or other information as needed to specifically locate, identify and revise or amend the existing Mining and Reclamation Plan. Include page, section and drawing numbers as part of the description.

DETAIL	LED SCHEDUL	E OF CHANG	GES TO THE MINING AND RECLAMATION PLAN
			DESCRIPTION OF MAP, TEXT, OR MATERIALS TO BE CHANGED
□ ADD	× REPLACE	C) REMOVE	p.i, Summary: Changed submission date, referred to updated DOGM Rules.
□ ADD	x REPLACE	□ REMOVE	p.ii., Introduction: Increased annual limestone production to 1.2 Mt/yr.
□ ADD	× REPLACE	□ REMOVE	p. v. Revised construction and production dates.
C) ADD	× REPLACE	C) REMOVE	p. vi-vii, Introduction: Updated chronology and the list of changes in the NOI.
□ ADD	x REPLACE	□ REMOVE	p.105-1, §105.1: Updated Base Map aerial photography date. Noted that some of the Chaffin Quarries have been mined through.
□ ADD	x REPLACE	D REMOVE	p.105-2, §105.3.11: Updated reference to revised map.
× ADD	C) REPLACE	☐ REMOVE	p.105-3, §105.3.14: Added text to explain that some pre-law quarries have been and would be mined through during expansion.
ממג ב	× REPLACE	☐ REMOVE	p.105-4, §105.3.15: Changed text to accurately describe map.
EI ADD	× REPLACE	□ REMOVE	p.105-4, 105-5 \$105.3.16: fixed typo, added reference to more recent slope stability report.
□ ADA	× REPLACE	□ REMOVE	p.105-6,7 §105.3.17: Updated description of revised Map R647-4-113 (Appx. 10).
C ADD	× REPLACE	□ REMOVE	p.105-7, §105.3.18: Removed references to the sequence of mining operations maps, as advised by DOGM. Replaced text with a reference to the ultimate mining map. Also revised total mine production amount.
CI ADD	x REPLACE	O REMOVE	p.105-8, §105.4: Change text to refer to an updated aerial photo.
× ADD	x REPLACE	× REMOVE	p.106-3, \$106.2: Updated map references, updated text to mention rock waste dump that is currently being used. Deleted redundant text.
CD ADD	× REPLACE	□ REMOVE	p. 106-4 to p. 106-19, §106.3: Drawings 4-106-1 through 4-106-12, Mine Progress Maps: Removed as directed by DOGM and replaced with Drawing 4-106-1: Ultimate Mine Map.
× ADD	× REPLACE	□ REMOVE	p. 106-4 to p. 106-19, §106.3: Replaced drawings 4-106-9-1 (Cross Section A-A') and 4-106-9-3 (Cross Section B-B') with Figures 4-106.9-1A, IB, and IC, Geologic Cross Sections of the Central, Northeast and Southwest Blocks, respectively.
□ ADD	☐ REPLACE	× REMOVE	Figures 106.9-2 and 106.9-4: These figures are not required. The information in these figures is presented in The Ultimate Pit Map and its associated cross sections.
□ ADD	x REPLACE	D REMOVE	p.106-20, §106.3: Revised quarry disturbance acreage.
□ ADD	× REPLACE	☐ REMOVE	p.106-3, 106-20, §106.3: Revised life of quarry disturbance acreage.
[] ADD	x REPLACE	C) REMOVE	p.106-22, §106.5: Updated Figure 4-106-5 (Soil Survey Map) with new proposed Life of Quarry Disturbance Limit.
CI ADD	x REPLACE	[] REMOVE	p.106-27, §106.9: Updated text to discuss rock waste dump located west of the crusher.
□ ADD	x REPLACE	C) REMOVE	p.107-3, §107.2: Updated text to discuss constructed sediment pond that controls runoff from the waste rock dump.
x ADD	C REPLACE	□ REMOVE	p.109-1, \$109.2: Added language to incorporate SW expansion into biological resource assessment.
x ADD	I) REPLACE	[] REMOVE	p.109-3, §109.4: Added reference to more recent slope stability report.
CJ ADD	× REPLACE	() REMOVE	p.111-3, Table 4-111-2-1: Updated reclamation channel peak flow for RC-1, based on revised ultimate pit.
CI ADD	x REPLACE	C) REMOVE	p.112-1, 112-2, §112: Updated reference to drawings, updated variance request.
x ADD	O REPLACE	C) REMOVE	p.112-2, 112-3, §112.1.13: Added findings from more recent slope stability report.

• ADD	× REPLACE	• REMOVE	p.113-1,2 §113.1: Revised disturbed area acreage and corresponding surety amount.	
ED ADD	× REPLACE	• REMOVE	Appendix No. 1: Drawing No. R647-4-104.3L, Updated Land Ownership Map.	
CICA []	x REPLACE	• REMOVE	Appendix No. 2: Drawing No. R647-4-105.1Ba, Updated Base Map.	
□ ADD	× REPLACE	• REMOVE	Appendix No. 3: Drawing No. R647-4-105.4, Updated aerial photo.	
□ ADD	× REPLACE	• REMOVE	Appendix No. 5: Drawing No. R647-4-105.2Q, Updated Surface Facilities-Quarry Map.	
• ADD	× REPLACE	• REMOVE	Appendix No. 7: Drawing No. R647-4-107.2, Updated Drainage Control Map.	
D ADD	× REPLACE	• REMOVE	Appendix No. 8: Drawing No. R647-4-105.3.17, Updated Proposed Reclamation/ Revegetation Area Map	
• ADD	× REPLACE	REMOVE	Appendix No. 9: Drawing No. R647-4-109, Updated Life of Quarry Disturbance Map.	
• ADD	x REPLACE	• REMOVE	Appendix No. 10: Drawing No. R647-4-113, Updated Comparison of Original Bonded Area to Present Disturbance Limit Map.	
× ADD	• REPLACE	• REMOVE	Appendix No. 16: Attached an additional rock slope stability report.	

I hereby certify that I am a responsible official of the applicant and that the information contained in this application is true and correct to the best of my information and belief in all respects with the laws of Utah in reference to commitments and obligations, herein.

Bruce Newell Plant Manager

Leamington Plant, Ash Grove Cement Company

July 9, 2008

FOR DOGM USE ONLY:
File #: M/ /
Approved:
Bond Adjustment: from (\$)
to \$
1.00

Return to: State of Utah Department of Natural

Resources Division of Oil, Gas and Mining 1594 West North Temple, Suite 1210 Box 145801 Salt Lake City, Utah 84114-5801 Phone: (801) 538-5291 Fax: (801) 359-3940

OnFORMS/MR-REV-att doc Instructions - Amend or Revise Mining Plan Page 3 of 3 ASH GROVE CEMENT COMPANY LEAMINGTON PLANT AND QUARRY, UTAH

SUBMITTAL BY ASH GROVE CEMENT COMPANY TO THE UTAH DEPARTMENT OF NATURAL RESOURCES, DIVISION OF OIL, GAS AND MINING, OF NOTICE OF INTENTION TO REVISE MINING OPERATIONS, ASH GROVE CEMENT COMPANY, LEAMINGTON PLANT, M/023/004, JUAB AND MILLARD COUNTIES, UTAH.

The following states or refers to the section of the Division's Rules and is followed by Ash Grove's response to the requirements of the Rule:

R647-4-104. Operator(s), Surface and Mineral Owner(s).

104.1. The name, permanent mailing address, and telephone number of the operator responsible for the mining operations and reclamation of the site.

Response:

Ash Grove Cement Company Leamington Plant P. O. Box 51 Nephi, Utah 84648

Leamington Plant, Leamington, Utah 435-857-1212 Administrative Office 435-857-1288 Fax

104.2. The name, permanent mailing address, and telephone number of the surface landowner(s) and mineral owner(s) of all land to be affected by the operations.

Response:

Ash Grove Cement Company Leamington Plant P. O. Box 51 Nephi, Utah 84648

Leamington Plant, Leamington, Utah 435-857-1212 Administrative Office 435-857-1288 Fax

104.3. The federal mining claim number(s), lease number(s), or permit number(s) of any mining claims, or federal or state leases or permits included in the lands affected.

Response:

All proposed mining operations are conducted on land owned in fee by Ash Grove. There are no federal mining claims, lease numbers, or permit numbers of any mining claims, federal or state leases or permits, except for the Division's mining permit M/023/004, included in the lands to be affected within the Proposed Permit Boundary. The Proposed Permit Boundary is coincident with, and the same as, the boundary lines of property owned in fee by Ash Grove. A Land Ownership Map is included in Appendix No. 1 of this NOI to show property boundaries, mining claims, etc. on adjacent lands.

R647-4-105. Maps, Drawings & Photographs

105.1 Topographic base map, boundaries, pre-act disturbance.

Response:

A Topographic Base Map has been prepared at a scale of 1 inch to 400 feet. This Base Map was prepared from aerial photography flown in April 1998June 2006. The Base Map includes topography (20 foot contour interval) developed from aerial photography and shows the following as required by Sections 105.1.11 through 105.1.14 of the Rules:

Property boundaries of surface ownership of all lands which are to be affected by the mining operations. Ash Grove owns in fee all lands included within the Proposed Permit Boundary. These lands are shown on the Land Ownership map in Appendix No. 1 of this NOI;

Perennial streams, springs, and other bodies of water, roads buildings, landing strips, electrical transmission lines, water wells, oil and gas pipelines, existing wells, boreholes, or other existing surface or subsurface facilities within 500 feet of the proposed mining operations;

The Proposed route of access to the mining operations from Highway 132, the nearest publicly maintained highway, is shown on the Base Map in Appendix No. 2 of this NOI. This map is at a scale appropriate to show access; and

Known areas which have been previously impacted by mining or exploration activities within the proposed disturbed area are shown on the Surface Facilities - Quarry Map, located in Appendix No. 4 of this NOI. This map shows the location of eight-six small abandoned and inactive limestone quarries located within the Life-Of-Quarry Disturbance Limit (note that Quarries D and E have been mined through). These are known as the Chaffin Quarries and are identified as Quarry A through H. They were mined in the early 1900's and were in existence on the site prior to the original Permittee and the present Operator beginning mining and manufacturing activities. The Surface Facilities-Quarry Map also shows the location of a quartzite quarry that was previously mined by the Operator as a source of silica and other areas that the Operator has disturbed for mining operations.

These and other items required under Section R647-4-105.1 are shown on more detailed maps included in this NOI. Wells, post mine drainage, ponds, existing surface or sub-surface facilities, etc. have been included on separate drawings for clarity. A separate map has been prepared at a scale of 1 inch to 1,000 feet to show Land Ownership and is included in Appendix No. 1 of this NOI. The Topographic Base Map is included in Appendix No. 2 of this NOI.

105.2 Surface facilities map

Response:

A Surface Facilities - Plant Map has been prepared at a scale of 1 inch to 100 feet to identify and show the location of facilities, such as buildings, roads and other structures located within the cement manufacturing area of the Plant. This map also shows the location of utility easements, such as overhead electric transmission lines and natural gas pipelines and the Proposed Permit Boundary in the vicinity of the Plant. The Surface Facilities - Plant Map is included in Appendix No. 4 of this NOI.

A Surface Facilities - Quarry Map has been prepared at a scale of 1 inch to 400 feet to show the location of the current facilities, such as buildings and other structures, roads, crusher, etc. This map also identifies the Proposed Permit Boundary and the Present Limit of Disturbance, as of May 7, 1999, within the active limestone quarry area. The Surface Facilities - Quarry Map is included in Appendix No. 4 of this NOI.

105.3 Maps, Drawings or Cross Sections

105.3.11 Regraded slopes to be left at steeper than 2h:1v.

Response:

No slopes that are proposed to be re-graded will be left at steeper than 2h:1v. However, it is proposed, as previously approved by the Division for the Central reserve block in the quarry, that final, un-graded highwalls in the Northeast reserve block also will be left at steeper than 2h:1v. A variance will be requested from the Division for these final highwall areas in the Northeast reserve block, as shown in Drawings 4-106-11 and 4-106-12. Slopes from the out-of-pit waste rock disposal area, identified on Drawings 4-106-1 through 4-106-10, that are greater than 2h:1v will be re-graded.

105.3.12 Plans, profiles and cross sections of roads, pads or other earthen structures to be left as part of the post mining land use.

Response:

All features, such as roads (except those to be left for property access) pads, ponds, or other earthen structures, currently used by Ash Grove will be reclaimed.

105.3.13 Water impounding structures.

Response:

All sediment control ponds and their associated surface diversion structures that have been constructed or that may be constructed in the future will be removed as part of the reclamation plan as described in section R647-4-110.

105.3.14 Maps identifying surface areas that will be disturbed but will not be reclaimed.

Response:

All surface areas that are disturbed will be reclaimed, except for the following:

- A. Standing final limestone highwalls (2v:1h maximum) and final shale highwalls (1h:1v maximum) in the Central, Southwest, and Northeast reserve blocks;
- B. Portions of the Ffinal quarry pit floors in the Central, Southwest, and Northeast blocks;
- C. A road leading north (the North road) from Highway 132 to the railroad; and
- D. A road leading south (the South road) from Highway 132 to the Quarry.

Standing highwalls will be left to provide potential habitat and cover for raptors and other wildlife species that may utilize these areas for shelter and nesting sites. The north and south roads will remain to provide access to the property and across the property by others who own property to the north and south.

Chaffin Quarries A, B, C, F, and H represent disturbances prior to 1975 and prior to our activities at the site. These Quarries have been left undisturbed except for Quarries B & C. These Quarries were used as temporary storage areas for kiln waste dust, which was a byproduct of our manufacturing process at the time the plant started. Dust was stored in this area because of the protection the limestone rock walls and floor provided. In 1989 our cement manufacturing process was changed and waste dust was no longer a byproduct. Since 1997 we have started recovering these storage piles by reclaiming the material back into our manufacturing process. By the year 2007 these waste piles will no longer exist and reclamation for Quarries B & C will be considered completed. It is not feasible to rip and seed the bottom of Quarries B and C because the bottom of the pits are solid rock and would provide no growth medium for the vegetation. Quarries D and E have been mined out, and Quarries B and C will eventually be mined out due to expansion of the Northeast Pit.

The areas that will be reclaimed and re-vegetated are shown on the map entitled "Reclamation Activities & Treatment, Proposed Area To Be Reclaimed and Re-vegetated" included in Appendix No. 6 of this NOI.

105.3.15 Sediment ponds, diversion channels, culverts.

Response:

A Drainage Control Map has been prepared at a scale of 1 inch to 400 feet on a topographic map base. This map shows the Proposed Permit Boundary, Life-of-Quarry Disturbance Limit, Proposed Pit Limits for the Central and Northeast reserve blocks and the Future Quarry Expansion Limit for the Southwest reserve block, existing and proposed ponds, and direction of drainage from the final pits. This Drainage Control Map is included in Appendix No. 7 of this NOI.

105.3.16 Baseline information maps and drawings

Response:

The following baseline information maps and drawings are also included in the Appendix Appendices of this NOI to provide additional information to the Division and to assist in making a determination of existing pre-mining conditions, operations, reclamation and post-mining land use:

- 1. A map entitled "Geology of the Champlin Peak Quadrangle, Juab and Millard Counties, Utah", prepared by Janice M. Higgins, is included in Appendix No. 8. This map is included to provide information on the geology of the Quarry and a description of the limestone and shale units to be mined.
- 2. A report entitled "Soil Conservation Service Soil and Vegetation Survey", prepared by the U.S. Department of Agriculture, Natural Resources Conservation Service, is included in Appendix No. 11. This report is included to provide additional site-specific information on soils in the vicinity of the Quarry as a supplement to the soil information presented in the Fairfield-Nephi Soil Survey and vegetation based on observations made in the vicinity of the Plant and Quarry.
- 3. A report entitled "Biological Assessment for Threatened, Endangered, and Proposed Species for the Proposed Ash Grove Cement Plant Expansion", prepared by the U.S. Department of Agriculture, Forest Service, Fishlake National Forest, Fillmore Ranger District, is included in Appendix No. 12. This report is included to provide information on the biological assessment

completed to analyze and evaluate the potential effects of the Quarry on the threatened, endangered and proposed species that may occur in the vicinity of the Plant and Quarry.

- 4. A report entitled "Biological Evaluation for Sensitive Plant and Animal Species for the Proposed Ash Grove Cement Plant Expansion", prepared by the U.S. Department of Agriculture, Forest Service, Fishlake National Forest, Fillmore Ranger District, is also included in Appendix No. 12. This report is included to provide information on the biological evaluation completed to analyze and evaluate the potential effects of the Quarry on the sensitive plant and animal species that may occur in the vicinity of the Plant and Quarry.
- 5. A report entitled "Surface Drainage Martin Marietta Cement Plant, Leamington, Utah", prepared by Rollins, Brown and Gunnell, Inc., is included in Appendix No. 13. This report is included to provide background information on soils and hydrology of the small surface drainage area in the vicinity of the Plant into which drainage from the Quarry flows.
- 6. A report entitled "1993-94 Annual Report of Findings and Water Withdrawals", prepared by Kubal-Furr & Associates, is included in Appendix No. 14. This report is included to provide information on the monitor wells installed on the Plant and Quarry. The information in this report includes identification numbers, locations, dates of installation and water-level measurements.
- 7. A Two reports entitled "Initial Evaluation Highwall Slope Stability Hank Allen Quarry, Ash Grove Cement Company, Juab and Millard Counties, Utah", and "Highwall Stability Evaluation: Ultimate Pit Slope Angles, Hank Allen Quarry Leamington Plant, Central and Northeast Block Pits, Juab and Millard Counties, Utah" were prepared by Seegmiller International, is and are included in Appendix Appendices Nos. 15. and No. 16 This The reports is are included to provide the following information on the limestone and shale materials at the Quarry including the following:
 - (A) The preliminary A detailed evaluation of the stability variables including geologic discontinuities, rock mass, shear strength and groundwater; and
 - (B) Analysis of the stability of various slope areas for planar, wedge, toppling and rotational shear failure.
 - (C) Recommendations for highwall design based on slope stability analyses.

105.3.17 Reclamation activities and treatment map

Response:

A map entitled "Reclamation Activities & Treatment Proposed Area To Be Reclaimed and Revegetated" has been prepared at a scale of 1 inch to 400 feet. This map is included in Appendix No. 6 of this NOI.

The Reclamation Activities and Treatment map shows the aerial extent of the present Quarry and the location of related Quarry facilities, such as the crusher and conveyor. The map also identifies the final dump toe of the waste rock storage area, the Plant "manufacturing area", existing ponds, a new proposed pond, and roads, etc. Proposed areas to be reclaimed and re-vegetated by the Permittee are also shown on the map.

The operations described in the original mine permit application, which was submitted to the Division in December, 1979, estimated disturbance to be approximately 273 acres as follows:

DESCRIPTION	ORIGINAL	PERMIT	ACRES
Mfg. & Raw Mtl. Storage		45	
Quarry		177	
Quartzite Quarry		7	
Waste Dust Disposal		44	
	Total:	273 A	cres

A map entitled "Comparison of Original Bonded Area to Present Disturbance Limit" was constructed for this NOI. The purpose of this map is to show a comparison of: (A) the original disturbance area estimated by the original Permittee in 1979 to include 273 acres; (B) the 1992—2006 disturbance limit estimated to be approximately "218"392 acres and (C) the Present Proposed Limit of Disturbance of 589—731 acres. This map is included in Appendix No. 10 of this NOI. This map also shows the location of areas that total approximately 19 acres that the Operator has reclaimed and seeded.

In 1995 the Operator estimated that "...there are 220 acres of disturbed land...and it is projected that this number will increase to 300 acres over the next 8 years, and continue to increase throughout the life of the mine." This estimate did not include acreage for the proposed mining of the Northeast reserve block. Based on that observation, an estimated annual disturbance of 10 acres per year could be expected. However, this figure does not necessarily represent additional disturbed acreage. It is a combination of additional disturbed acreage and acreage disturbed by moving lower on the same bench, i.e. disturbing the same land but at greater depths.

The disturbance limit boundary has been revised and re-drawn to enclose all lands that currently have been disturbed. and certain undisturbed "island" areas that were not included in the disturbance limit boundary of the original mine permit application submitted in 1979.

The area of the Present Disturbance Limit Boundary was determined from aerial photography and its extent verified on the ground by the Operator. The disturbed acreage was determined by AutoCAD Map 2000 software. The Present Proposed Life of Quarry Limit of Disturbance boundary was determined to include 589-731 acres, as shown on the black and white aerial photograph of the Leamington Plant and Quarry included in Appendix No. 3 of this NOI.

The Reclamation Activity & Treatment Map identifies the boundary of the Proposed Life-Of-Quarry Disturbance Limit, which includes approximately 669-731 acres. The map also shows the extent of mining activities within this boundary. It is worth noting that although the Life-of-Quarry disturbance boundary encompasses 669-731 acres, not all of the acreage included within the boundary will be disturbed.

105.3.18 Other maps, plans, or cross-sections

Response:

A series of drawings, identified as Drawings 4-106-1 through 4-106-12, was prepared at a scale of 1 inch to 500-400 feet to represent the ultimate mine map. show the time sequence of the advance of mining operations during the period January 1999, through September 2059. These drawings illustrate the successive development of the quarry over time and the change in topographic contours of the Quarry area and the This map shows the maximum advance downward of the pit floor, and. The drawings also show the the approximate final dump toe for the proposed shale disposal area. These This drawings is are included in Section R647-4.106 of this NOI. Based on an extraction rate of 900,000 tons per year, the mine life is estimated at 109 years.

Two three-dimensional (3D) views illustrating the development of the quarry as of January 2004, and as of the year 2046, also have been prepared. These 3D views are included in Section R647-4-106 of this NOT.

Three we geologic cross-sections identified as Geologic Cross-Section A-A' Central Block, and Geologic Cross-Section B-B' Northeast Block, and Geologic Cross Section C-C' Southwest Block were prepared to show the relationship of the limestone and shale beds that will be mined. The geographic location of these geologic cross sections are indicated on Drawings 4-106-1 through 4-106-12. These cross-sections are included in Section R647-4-106 of this NOI as Figures 4-106.9-11A, 1B, and 1C and 4-106.9-3.

105.4 Photographs

Response:

A black and whitecolor aerial photograph, which was flown and taken on May 7, 1999June 11, 2006, is included in Appendix No. 3 of this NOI. This photograph shows the Present Limit of Disturbance Boundary for mining and manufacturing operations. The Operator has marked this Present Limit of Disturbance in the field on the ground.

R647-4-106. Operation Plan

106.1 Type of mineral(s) to be mined;

Response:

Limestone and shale will be mined for use as raw kiln feed for the manufacture of Portland cement. The stratigraphic nomenclature and the depositional relationships of these units are shown in Figure 4-106.1-1.

106.2 Type of operations to be conducted, including the mining/processing methods to be used.

Response:

The existing mining operation is an area surface mine operated for the quarrying of rock to be used as a raw material in the manufacture of Portland cement. Mining operations include drilling, blasting, loading broken rock, transportation of rock, crushing rock and rock storage. After being conveyed from the quarry operation, the rock is pulverized and blended with other raw materials to produce kiln feed for the manufacture of Portland cement. All mining operations are conducted by the use of conventional mining equipment, including drills, 100-ton haul trucks, dozers, grader, trackhoe, loaders, feeder breakers, belt conveyors and a stacker/reclaimer. No deleterious materials have been or are anticipated to be encountered during mining. Deleterious materials used as part of operations are handled appropriately, as detailed in Section 107.1.12. The following is a summary of the mining operation to be conducted:

MINE PLAN SUMMARY

The mine plans presented were developed from a recently updated computer geologic model. The model was prepared using two Minex software modules. The data imported into the software included all available core drill hole data, as well as chemical analysis from approximately 200 blast holes. Highwall geometries were designed to conform to the recommendations provided by rock slope stability analyses performed for the pit. The new geologic model provided more accurate design information for improved volumetrics, mine slope design and resource recovery estimates. The new model also used a topographic surface prepared from aerial photography flown in April 1998.

The outline of the mine plan focused on the Central and Northeast blocks of the limestone resource. The plan began at projected bench faces available at the beginning of January 2000. The quarry benches are designed to be 60 feet high with a face slope of 87 degrees. The final highwall slope is planned to be 63.4 degrees or 2.0 vertical to 1.0 horizontal when the final pit walls are in L4 and L3 limestones. A final pit slope, including the quarry end-walls, of 45 degrees (1v:1h) will be maintained where the quarry walls are in material other than the L4 or L3 limestones.

FIGURE 4-106.1-1 - STRATIGRAPHIC COLUMN

In order to minimize rockfall and rotational slope failure hazards, three 50-foot wide step-outs will be constructed on the south slope of the Central Pit at the 5,800-, 5,500-, and 5,300- foot elevations.

Approximately 1,200,000900,000 tons of limestone are scheduled to be recovered each year. The total resource recovery for the life of the mine plan is estimated to be approximately 75-98 million tons. The new mine design does not neutralize additional limestone reserves projected to be located to the southwest of this proposed mine plan. The quarry life is estimated to be 62-109 years. However, it should be noted that certain conditions could exist that may affect the rate of extraction of the resources, as well as the sequencing and benching plan that has been developed. These conditions may include, but are not be limited to, economical, geological and/or physical constraints.

The shale removed from between the limestone beds and any poor quality limestone has been disposed of in a shale disposal site adjacent to the crusher location. Under current mining conditions, approximately 85,000 cubic yards of waste rock is stockpiled at this location annually. Eventually, additional waste rock storage locations will be required, such as on the pit floor, which will be submitted for approval in updated versions of this NOI. By year 2018, the waste area will have accumulated approximately 1.1 million tons of waste material. Starting in year 2019, sufficient room will be available in the mined out area of the central quarry to accommodate future waste material. The top surface elevation of the shale dump will be the 5,400 foot level. The length of the long axis of the dump area will be from north coordinate N446200 to N444000.

The quarry operations will drill and blast the rock prior to excavation. A loader and off-highway trucks will remove the blasted material to either the waste dump site or the current in-pit crusher. Support crawler dozers, graders, water trucks and utility trucks will be used to maintain the roads and surfaces needed by the mobile production equipment.

106.3 Estimated acreages proposed to be disturbed and/or reclaimed annually or sequentially.

Response:

The life of the proposed Quarry operation, as presently planned, will extend for a period of about $\frac{62-109}{2}$ years. The proposed operations will disturb approximately 229 acres within the pit and 28 additional acres in the area immediately surrounding the pit.

FIGURE 4-106-9-1 - CROSS-SECTIONAL VIEW CENTRAL RESERVE BLOCK

REPLACED WITH FIGURES 4-106-9-1A,1B,1C

DRAWING 4-106-2 - CENTRAL RESERVE BLOCK

DRAWING 4-106-3 - CENTRAL RESERVE BLOCK

DRAWING 4-106-4 - CENTRAL RESERVE BLOCK

DRAWING 4-106-5 - CENTRAL RESERVE BLOCK

DRAWING 4-106-6 - CENTRAL RESERVE BLOCK

DRAWING 4-106-7 - CENTRAL RESERVE BLOCK

DRAWING 4-106-8 - CENTRAL RESERVE BLOCK

DRAWING 4-106-9 - CENTRAL RESERVE BLOCK

DRAWING 4-106-10 - CENTRAL RESERVE BLOCK

FIGURE 4-106-9-2 - 3-D VIEW CENTRAL RESERVE BLOCK

FIGURE 4-106-9-31A,1B,1C - CROSS-SECTIONAL VIEW CENTRAL, NORTHEAST, AND SOUTHWEST RESERVE BLOCKS

DRAWING 4-106-11 - NORTHEAST RESERVE BLOCK

DRAWING 4-106-12 - NORTHEAST RESERVE BLOCK

FIGURE 4-106-9-4 - 3-D VIEW NORTHEAST RESERVE BLOCK

limestone and shale. Additionally, other lands will be disturbed for the construction of roads, ponds, and mining facilities. A total of 669-731 acres are included in the proposed Life-Of-Quarry Disturbance Limit, to be affected over the 62109-year life of the Quarry. Therefore, the proposed mining operations will affect about 11 acres of land annually over the life of the quarry operation. However, because of the method of mine advance is downward to progressively lower benches, as well as laterally, the quarry operations do not actually disturb this additional amount of land each year.

Due to the geology of the limestone deposit, i.e. vertical beds, and the nature of the mining operation, the mine generally advances downward over time from the top of the mountain through the vertical limestone beds to progressively lower levels. Gradually, the mine advances laterally into adjacent limestone and shale beds. This method of mining lessens the annual lateral advance of the quarry operation. Therefore, the annual acreage disturbed usually represents an advance to a lower bench level and not necessarily a disturbance of additional acreage. This mining method contains the mining operation in a smaller area but for a longer period of time.

106.4 Nature of materials to be mined, waste and estimated tonnages.

Response:

The materials to be mined are limestone, interbedded with silty, calcareous, phyllitic shales. The mine produces about 900,000 tons of limestone and about 130,000 tons (89,000 cubic yards) of waste rock (shale) annually. Due to the steep topography and thin soils in the area, it is not practical to stockpile topsoil.

Table 4-106.4-1, Total Schedule Quality Report for the Life of Quarry, provides estimates of the volume and tonnages of limestone and shale to be mined and removed. This table shows these quantities by year and by stratigraphic interval, i.e. limestone L3 and shale S3, over the proposed life of the Quarry. The table also shows the quality of the rock resources as determined from the computer block model. The Operator has marked this table CONFIDENTIAL and requests that this information be held CONFIDENTIAL under the provisions of Section R647-4-115 of the Division's Rules.

106.5 Existing soil types.

Response:

The existing soils in the Proposed Permit Boundary are described in the June 1984 report entitled "Soil Survey of Fairfield-Nephi Area Utah, Parts of Juab, Sanpete and Utah Counties" (the NRCS soils survey), prepared by the United States Department of Agriculture, Soil Conservation Service (now Natural Resources Conservation Service). The soil map units in the area of the Quarry are shown on the Soil Survey Map, included as Figure 4-106-5 in this section of the NOI.

		Table	Table 4-106.4-1										
	ASH GROVE CEMENT COMPANY- LEAMINGTON MARRY UTAH TOTAL SCHEDULE MALITYREPORT FOR THE LIFE-OF-MARR	OVE CEMENT COMPANY- LEAM!	VY- LEAMING	TON I	NGTON QARRY UTAH THE LIFE-OF-QARRY								
CONFIDENTIAL													_
PERIOD AND LOCATION	SHALE (TONS)	IN PLACE SHALE (193)	SHALE AS WASTE ROCK (B3)	BED	LIMESTONE (TONS)	Cab S	Ogw %)	K20	Ma ₂ O	¥e₂0₃	SiO ₂	A120,	
2008-2013 EST, ANNUAL PRODUCTION	129,000	57,912	86,869		907,000				I				_
				1.3	217,680	51.11	1.58	0.27	0.11	0.48	3.09	1.54	_
NORTHEAST PIT				1.4	507,920	50.24	1.78	0.32	0.09	0.36	4.73	1.02	_
	3,870	1,737	2,606	\$2		15.04	1.92	2.99	0.24	6.39	38.24	19.20	_
	34,830	15,636	23,455	53		27.99	2.03	2.77	0.20	3.68	26.57	11.59	_
				L3	18,140	51.11	1.58	0.27	0.11	0.48	3.09	1.54	_
CENTRAL/SOUTHWEST PITS				1.4	163,260	50.24	1.78	0.32	0.09	0.36		1.02	_
	90,300	40,539	60,808	83		27.99	2.03	2.77	0.20	3.68	26.57	11.59	_
LIFE OF GARRYEST. TOTAL PRODUCTION	27,611,148	12,395,577	18,593,366		97,920,895								
				Li	8,008,544	49.89	2.13	0.37	90.0	0.52	3.87	1.27	
				L2	2,501,806	44.81	2.23	0.59	0.21	1.41	8.73	3.88	_
				1.3	5,994,866	51.11	1.58	0.27	0.11	0.48	3.09	1.54	_
NORTHEAST PIT				L4	17,257,556	50.24	1.78	0.32	0.09	0.36	4.73	1.02	_
	1,874,778	841,651	1,262,476	S1		15.14	1.96	3.19	0.45	5.54	38.59	17.44	
	781,799	350,976	526,464	82		15.04	1.92	2.99	0.24	6.39	38.24	19.20	
	4,072,982	1,828,499	2,742,749	83		27.99	100	2.77	0.20	3.68	26.57	11.59	
	10/10/10/10/10/10/10/10/10/10/10/10/10/1			1.3	23,966,634	51.11	1.58	0.27	0.11	0.48	3.09	1.54	_
CENTRAL/SOUTHWEST PITS				1.4	40,191,489	50.24	1.78	0.32	60.0	0.36	4.73	1.02	
	20,881,590	9,374,451	14,061,677	83		27.99 2.03	2.03	2.77	0.20	3.68	26.57	11.59	

The life of quarry total production was calculated by finding the volume between the ground surface surveyed June 2006 and the ultimate mine map contours presented in the March 2007 NOI. The volumes were calculated using AutoLand Desktop Design 2007 AutoCAD Software
Shale tonnages (2008-2013) are taken from the tonnage of material stockpiled as waste rock and may actually contain up to 15% limestone
Shale tonnages (Life of Quarry) are taken from the calculated volume of shale as determined by drillhole data
Shale volumes are calculated from tonnages assuming a density of 165 pcf for in-place shale and a density of 110 pcf for waste rock 2008-2013 estimated annual production based on 2007 production. Actual production may vary depending on market conditions.

The NRCS soil survey generally describes the soils in the area of the existing and proposed mining operations as dominantly well drained and somewhat excessively drained, sloping to very steep soils and barren rock outcrop on hillsides, ridges, and mountainsides.

More specifically, the soils identified in the area of the existing and proposed mining operations are as follows:

```
Rhf - Rock outcrop-Lodar complex (30 to 70 percent slopes);
Ldf - Lodar-Rock outcrop complex (30 to 70 percent slopes);
Ddc - Donnardo stony loam (2 to 8 percent slopes); and
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PK - Pits-Dumps complex.

The majority of the area affected by the existing and proposed quarry operations is mapped as Rock outcrop-Lodar complex (Rhf) with 30 to 70 percent slopes and Lodar-Rock outcrop complex (Ldf) with 30 to 70 percent slopes. The remaining area is mapped as Donnardo stony loam (Ddc) with 2 to 8 percent slopes and Pits-Dumps (PK) complex. These existing soil complexes are described as follows:

Rock outcrop-Lodar complex (Rhf).

This map unit is on hillsides. Slopes are long and convex. In most areas the present vegetation is mainly grasses and shrubs. The unit is about 70 percent Rock outcrop and 20 percent Lodar very cobbly loam, 30 to 70 percent slopes. The components of this unit are so intricately intermingled that it was not practical to map them separately at the scale used. Included in this unit are about 5 percent Amtoft stony loam, moist, 30 to 70 percent slopes; and 5 percent Saxby very cobbly loam, moist, 30 to 70 percent slopes, both on south-facing hillsides. The Lodar soil is shallow and somewhat excessively drained. It formed in colluvium and residuum derived dominantly from limestone. Rock outcrop consists of exposures of barren bedrock, mainly on escarpments and ridges. This unit is used for wildlife habitat.

Lodar-Rock outcrop complex (Ldf).

This map unit is on hillsides. Slopes are long and convex. In most areas, the present vegetation is mainly grasses and shrubs. The unit is about 60 percent Lodar very cobbly loam, 30 to 70 percent slopes, and 20 percent Rock outcrop. The components of the unit are so intricately intermingled that it is not practical to map them separately at the scale used. Included in this unit are about 10 percent Lodar very cobbly loam, 3 to 30 percent slopes on hillsides; and 5 percent Borvant cobbly loam, 8 to 25 percent slopes on alluvial fans.

Permeability of the Lodar is moderate. Available water capacity is about 1 to 1.5 inches and water supplying capacity is 2 to 4 106-23

inches. Effective rooting depth is 10 to 20 inches. The organic content of the surface layer is 1 to 4 percent. Runoff is medium and the hazard of erosion is slight. The Rock outcrop consists of exposures of barren rock, mainly on escarpments and ridges. This unit is used as rangeland and for wildlife habitat.

Donnardo Stony loam (Ddc).

This very deep, well-drained soil is on alluvial fans. The soil is formed in alluvium derived dominantly from sandstone, limestone and quartzite. Slopes are medium in length and are convex. In most areas, the present vegetation is mainly grasses and shrubs. Included in this unit are about 5 percent Donnardo stony loam, 8 to 25 percent slopes; 5 percent Pharo very stony loam, 3 to 10 percent slopes; 5 percent Borvant cobbly loam, 2 to 8 percent slopes; and 5 percent Juab loam, 2 to 4 percent slopes.

Permeability of the Donnardo soil is moderately rapid. Available water capacity is about 4.5 to 7 inches. Water supplying capacity is 6 to 9 inches. Effective rooting depth is 60 inches or more. The unit is used as rangeland and wildlife habitat.

Pits-Dumps complex (PK).

This map unit consists mainly of mine pits and associated tailing dumps. Unless it is reclaimed, this unit generally produces very little vegetation and is severely limited for most uses.

106.6 Plan for protecting and redepositing existing soils.

Response:

The soils, as described above, in the proposed mining area are not prime farmland soils and are generally rocky and poorly developed. It is considered impractical in most cases to The Operator does not propose to remove, store and redeposit any existing soils due to the combination of thin, poorly developed soils and steep slopes surrounding the pit. When practical, the operator will place topsoil in bermed, revegetated, stockpiles so that it can be redeposited during reclamation.

106.7 Existing vegetative communities.

Response:

The original permit application contained an Environmental Assessment Input report prepared by Mr. Benton M. Smith, Range Conservationist with the Fillmore Ranger District, Fishlake National Forest. A copy of this report is included in Appendix No. 11 of this NOI. This Environmental Assessment Input report summarized the range resource within the area, which was proposed to be affected by the mining operation and described the range resource as follows: "The range resource within the area which would be affected by the proposal consists of the following:

Vegetation Type	Condition	Approximate Acres
Suitable sagebrush	Poor	230
Unsuitable browse-shrub	Good	30
Unsuitable-pinyon-juniper	Poor	200
Barren	-	_70
	Total	530

Range analysis records indicate that the sagebrush type produces about 223 lbs/acre of air-dry forage. Assuming that the forage is all available to livestock and allowing 50 percent utilization of the forage on the suitable sagebrush type, this produces approximately 25 animal unit months of feed per year, or 5 percent of the current grazing obligation on the Fool Creek Allotment. However, due to the lack of available water on this part of the allotment, cattle are not able to fully utilize the forage in this draw, except for short periods following rainstorms. This lessens the importance of the area for livestock grazing.

Range conditions and grazing use are expected to remain relatively unchanged in the foreseeable future except for natural, successional changes. The potential for vegetation manipulation to improve the forage production is good, but the potential to develop water for livestock on the National Forest land is poor."

Mr. Benton M. Smith further reported, "No threatened or endangered plants are known to grow in the area."

According to the NRCS soil survey of Fairfield-Nephi Area, Utah, prepared by the United States Department of Agriculture, the soil units mapped on the area of the present and proposed quarry include the following:

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Rhf - Rock outcrop-Lodar complex (30 to 70 percent slopes);
Ldf - Lodar-Rock outcrop complex (30 to 70 percent slopes);
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Ddc - Donnardo stony loam (2 to 8 percent slopes); and

PK - Pits-Dumps complex.

The potential plant community on these soil complexes is as described by the U. S. Department of Agriculture as follows:

1. Rhf - Rock outcrop-Lodar complex (30 to 70 percent slopes). This unit is about 70 percent Rock outcrop which consists of exposures of barren bedrock, mainly on escarpments and ridges. The remaining 30 percent of the unit is Lodar very cobbly loam. The potential plant community on the Lodar is about 65 percent perennial grasses, 10 percent forbs,

and 25 percent shrubs. Important species are:

Bluebunch wheatgrass Black sagebrush Nevada bluegrass Sandberg bluegrass Indian ricegrass

Because of the steepness of slope and the shallow depth of soil, grazing management practices are poorly suited to this unit.

2. Ldf - Lodar-Rock outcrop complex (30 to 70 percent slopes). The potential plant community on this soil is about 65 percent perennial grasses, 10 percent forbs, and 25 percent shrubs. Important species are:

Bluebunch wheatgrass Black sagebrush Nevada bluegrass Indian ricegrass

Because of the steepness of slope and the shallow depth of soil, grazing management practices are poorly suited to this unit.

3. Ddc - Donnardo stony loam (2 to 8 percent slopes).

The potential plant community on this soil is about 65 percent perennial grasses, 15 percent forbs, and 20 percent shrubs. Important plant species are:

Wyoming big sagebrush Bluebunch wheatgrass Indian ricegrass

This unit is suited to range seeding. The main limitation is the content of rock fragments. Plants suitable for seeding include Whitmar wheatgrass, slender wheatgrass, and species of the plant community for which seed or stock is available.

4. PK - Pits-Dumps complex.

Unless it is reclaimed, this unit generally produces very little vegetation and is severely limited for most uses.

106.8 Depth to groundwater, extent of overburden and geologic setting.

Response:

The depth to groundwater level is measured on an approximate quarterly basis in the Plant water supply well (USGS well number

(C-14-3) 33bbb-2). The depth to water level recorded on March $\frac{35}{1999}$ 2007 was $\frac{43.7746.1}{1999}$ feet below the land surface datum of 4,828 feet. The depth to water level has averaged 44.5 feet below the land surface datum over the period January 24, 1994, to March $\frac{35}{1999}$, $\frac{19992007}{19992007}$.

The depth of the overburden, as indicated by the Fairfield-Nephi area soil survey report, the type of soil map units in the area of the Quarry and actual mining experience varies from several feet to zero feet. In many areas of the Quarry, bare rock is exposed with little or no overburden present.

The limestone beds mined at the quarry are of Cambrian Age. The beds have been overturned and are near vertical, as shown in the geologic cross-sections included in this submittal. The limestone beds are interbedded with phyllitic shales and calcareous siltstones. The stratigraphic relationships of the limestone and shale beds are shown on the Stratigraphic Column, Figure 4-106.1-1, previously referenced in this section of the NOI. The Dome Limestone Formation, referred to as L3 in this NOI, and the Swasey Limestone, referred to as the L4 limestone, will be the principal limestone resource mined over the life of the Quarry. The Whirlwind Shale, referred to as the S3 shale, lies between the L3 and L4 limestone beds. The S3 shale will also be mined. The lowermost shale, the Pioche Formation, is underlain by the Tintic Quartzite. This quartzite has been mined on site in the past by the Operator for use as a silica source. The quartzite is not presently mined, but may be mined in the future as a supplemental source of silica.

106.9 Proposed location and size of ore and waste stockpiles, tailings facilities and water storage/treatment ponds.

Response:

There are no tailings facilities or water storage/treatment ponds located on the Quarry site.

The limestone and shale mined from the Quarry are transported by conveyor to a central storage area and stacker located adjacent to the Plant. The location of this storage area is shown on the Surface Facility - Plant Map included in Appendix No. 4 of this NOI.

The revised mine plan for the Quarry proposes the construction of oOne out-of-pit waste rock disposal area has been constructed. This stockpile will be located adjacent to and west of the present crusher and conveyor belt line. The waste stockpile will begins at an elevation of about 5,380 feet, extends downslope to an elevation of about 5,125 to 5,360 feet, and contains approximately 405,000 cubic yards of material. The waste stockpile will extend downslope to the approximate final dump too at an elevation varying from 5,100 to 5,340 feet and ultimately extend approximately 2,500 feet to the southwest from the present conveyor belt line and will have a capacity of approximately 1,000,000 cubic yards. Pond #7 accepts all runoff from the stockpile. 106-27

R647-4-107. Operation Practices.

107.1 Public safety and welfare.

107.1.11 Closing or guarding of shafts and tunnels.

Response:

There are no shafts or tunnels known to the Operator to exist within the Proposed Permit Boundary.

107.1.12 Disposal of trash.

Response:

Waste material at the Leamington Plant and Quarry, depending on the nature of the material, is disposed of by a variety of generally acceptable practices as described below:

MATERIAL Used oil	DISPOSAL METHOD Offsite disposal by commercial recycler (Advanced Petroleum RecyclingSafety Kleen)
Heavy greases	Offsite disposal by commercial recycler (Safety Kleen Van Waters and Rogers)
Solvents (Safety Kleen)	Offsite disposal by commercial recycler
Paint wastes (Van Waters and Rogers)	Offsite disposal by commercial recycler
Process waste water Storm water	Used for cooling in on-site mills Granted "Total ContainmentNon-Discharge Status" by Utah Department of Environmental Quality Division of Water Quality.
Scrap metal and empty drums	Offsite disposal (Swenson-Western Metal Salvage)
Office waste and General trash	Millard County Landfill (haulage by delta garbage service)
Used refractory material	Recycled through the kiln as raw material (No chrome brick)
Plant sweepings From pavement sweeper	Recycled through the kiln.
Fabric filter dust collector bags	Juab County Landfill 107-1

Biodegradable vegetation material that has been grubbed and cleared from the Quarry site may be buried in the waste rock disposal area. Materials that can be salvaged, including tires, metal, etc., are reclaimed and transported off site for disposal by a commercial recycler. For example, waste oils are collected and picked up by a contractor and transported off site for recycling.

All hazardous materials are stored and handled appropriately. They are clearly labeled, stored in designated locations, and disposed of within 180 days. Hazardous wastes are stored in the Universal Waste Storage Building next to the Control Center and in a designated storage shed next to the crusher. The facility complies with an approved Spill Prevention Control and Countermeasures Plan (SPCC) which requires that specific operating procedures, control measures, and countermeasure plans be followed.

107.1.13 Plugging or capping of drill, core holes.

Response:

All drill and core holes, except for blast holes, are plugged or capped immediately after drilling. The locations of known drill holes are shown on the Geologic Control Map included in Appendix No. 8 of this NOI. There are four monitor wells (SWDA-1, SWDA-2, SWDA-3 and SWDA-5) located in the Quarry that have not been plugged. These monitor wells are still in use and are enclosed by a metal surround and locked. The Operator is not aware of any other drill or core holes located within the Proposed Permit Boundary that have not been properly plugged or capped. If a hole is located, in the future, that has not been plugged or capped, the Operator will notify the Division and plug the hole in accordance with applicable rules and regulations.

107.1.14 Posting of appropriate warning signs. Response:

The Operator will post signs around the Proposed Permit Boundary advising the public the property is owned by Ash Grove Cement Company and is the site of a quarry operation.

Additionally, the Operator will mark the location of the Present Disturbance Limit Boundary by the use of steel T-posts driven in the ground. A piece of white PVC pipe will be placed over the T-posts to increase visibility. This will provide a visible line-of-sight marking of the Present Disturbance Limit Boundary.

Within the Present Disturbance Limit Boundary, the Operator also has posted signs in the active Quarry area to warn of blasting and other site-specific conditions. Dangerous highwall warning signs have been posted wherever they are considered safe to install.

107.1.15 Construction of berms, fences and/or barriers. Response:

Berms, fences and/or barriers are constructed as required by the Mine Safety and Health Administration (MSHA) pursuant to the Federal Mine Safety and Health Act of 1977 and at such other locations that may be required by the Division for safety purposes.

107.2 Drainages.

Response:

There are two small intermittent, rocky stream beds located within the Proposed Permit Boundary. These stream beds drained into the Sevier River prior to the conduct of mining and manufacturing activities. Any All runoff from presently disturbed areas within the Proposed Permit Boundary, except for runoff from the area immediately west of the rock storage facility, is channeled into and retained by six seven existing sediment ponds.

Any All runoff from the area immediately west of the rock storage facility would flows down stream and off the Proposed Permit Boundary. Ainto a new sediment pond (Pond #7), which the Operator estimates to be measuring approximately 4.13 surface acres in size., will need to be constructed to contain runoff in this area. The Operator is currently workingworked with the State of Utah Department of Environmental Quality, Division of Water Quality (DEQ) in to sizing size and permitting the construction of this pond. Design calculations for this pond have been included in Appendix 13 of this NOI. Expected completion of the pond is anticipated sometime in the year 2002. The Operator shall take appropriate measures to avoid or minimize environmental damage in these areas.

107.3 Erosion control.

Response:

Operations shall be conducted in a manner such that sediment from disturbed areas is adequately controlled. The Operator will utilize appropriate erosion control measures, including but not limited to, the use of silt fencing, straw or hay bale check dams, rock check dams and/or rock riprap drop structures to control erosion in disturbed areas. Typical profiles and cross-sections illustrating the installation of these measures and structures are shown in Figures 4-107.3-1 through 4-107.3-4 in this section of this NOI.

107.4 Deleterious material.

Response:

There is no deleterious or potentially deleterious material known to exist within the area to be mined that will be removed and would result in adverse environmental affects. Handling, disposal, and storage of deleterious materials used as part of operations are discussed in Section 107.1.12.

107.5 Soils.

Response:

As discussed in Section R647-4-106.5 of this NOI, the existing soils are thin to absent, cobbly to pebbly, and for the most part

FIGURE 4-107.3-1 - STRAW OR HAY BALE CHECK DAM

FIGURE 4-107.3-2 - ROCK CHECK DAM

FIGURE 4-107.3-4 - TYPICAL ROCK RIPERAP DROP STRUCTURE - CROSS SECTION VIEW

are poorly suited for agricultural use. Utilization of the existing soils is further limited by the steepness of the slopes and low moisture conditions. The Operator does not believe it is practical, in most cases, to remove and store topsoil for use in future reclamation. Additionally, the long term nature of the Quarry operation could require storage of any topsoil that was removed for extended periods of time, i.e. up to 20 years or more. Although any desirable physical characteristics of the topsoil would remain, storage of topsoil for extended periods would result in a sterile medium, due to loss of the microbial assemblage. To the extent practicable, the Operator will remove suitable topsoil and store it in a stable condition so as to be available for reclamation.

107.6 Concurrent reclamation.

Response:

Due to the open pit nature of the Quarry operation and long-term mining in a relatively confined area, concurrent reclamation of the active pit is not practical. Areas that have been disturbed but are not routinely or currently utilized shall be kept in a safe, environmentally stable condition and protected from erosion. During operations, the Operator will reclaim other disturbed areas, such as drill sites, roads, etc. when they are no longer needed.

R647-4-108. Hole Plugging Requirements.

108.1.11 Setting a nonmetallic permaplug.

Response:

All holes, except blast holes, drilled by the Operator within the Proposed Permit Boundary will be plugged or capped in accordance with the Division's requirements.

108.1.12 Tillable farmland.

Response:

There is no tillable farmland located within the Proposed Permit Boundary.

108.2 Drill holes that encounter water.

Response:

A Geologic Control Map was prepared for this NOI to show the location of drill holes completed on the Quarry site. This map is included in Appendix No. 8 of this NOI. This map also shows the locations of monitor wells, piezometers, the Plant water supply well, survey control points, soil sample locations, outcrop points and other information.

Drill holes in the Quarry area do not typically encounter any appreciable amounts of water, other than percolation from the surface. The elevation of the active quarry is currently at and above the level of the crusher, at 5,380 feet above sea level. The elevation of the proposed final pit floor of the Quarry is projected to be at approximately 5,220 feet. This places the final pit floor considerably above the normal water table level in the vicinity of the Quarry. The water well that supplies the Plant is located at a surface elevation of 4,828 feet (top of casing). The water level in this well is measured on an approximate quarterly basis. The water varies from 53 feet below the top of the casing (4,775 feet above sea level) to 45 feet below the top of the casing (4,783 feet above sea level).

108.2.11 Artesian flow.

Response:

No artesian flow has been encountered in any of the drill or core holes completed within the Proposed Permit Boundary.

108.2.12 Significant nonartesian flow.

Response:

No significant non-artesian flow has been encountered in any of the drill or core holes completed within the Proposed Permit Boundary. Any hole that encounters significant amounts of nonartesian water will be plugged by the Operator in accordance with the Division's requirements.

108.2.12.111 50-foot cement plug.

Response:

Holes that encounter significant amounts of non-artesian flow shall be plugged by placing a 50 foot cement plug immediately above and below the aquifer(s); or

108.2.12.112 Filling from bottom up.

Response:

Holes that encounter significant amounts of non-artesian flow shall be plugged by filling from the bottom up (through the drill stem) with a high-grade bentonite/water slurry mixture. The slurry shall have a Marsh funnel viscosity of at least 50 seconds per quart prior to the adding of any cuttings.

R647-4-109 Impact Assessment.

109.1 Surface and groundwater systems.

Response:

The proposed mining operations are not expected to impact either the surface or the groundwater systems. Surface flow is minimum on the Quarry site. Most surface flow infiltrates rapidly as a result of the rocky nature of the site. The Plant is located in the mouth of a small watershed that has an area of 1.1 square miles. Any runoff from the Quarry site and Plant is collected in a series of sediment ponds and allowed to evaporate. These sediment ponds and associated diversion structures were constructed so as to allow our operation to be Granted "Total Containment Status" by the Utah Department of Environmental Quality, Division of Water Quality. Upon cessation of mining activities and as part of the reclamation plan as outlined in this NOI, these sediment ponds will be reclaimed. Also, it should be noted that no mining is proposed in the alluvial valley of the Sevier River.

As discussed in Section R647-4-108.2, the groundwater level is located considerably below the level of the current Quarry operations and the proposed level of the final pit floor at 5,220 feet.

109.2 State and federal threatened and endangered species.

Response:

There are no State or federally listed threatened or endangered species known to exist within the Proposed Permit Boundary. Dana L. Nall, District Wildlife Biologist with the U. S. Forest Service, Fishlake National Forest, Fillmore Ranger District (USFS) prepared a report in September 1994 entitled "Biological Assessment for Threatened, Endangered, and Proposed Species for the Proposed Ash Grove Cement Plant Expansion". A copy of this report is included in Appendix No. 12 of this NOI.

The purpose of this biological assessment was to analyze and evaluate the potential effects of Ash Grove's proposal to expand its existing operations to include approximately 145 acres of land that at that time was National Forest System lands. Ash Grove obtained title to these lands in the summer of 1998 in a land exchange with the U.S. Forest Service. It is assumed that the proposed development of the pit, including the 31-acre expansion of the southwest pit, will have no adverse effects on biological resources.

Nall states, in Section VII. Determination, of the Biological Assessment report: "As a result of this assessment it is my professional determination that the proposed Ash Grove Cement Plant expansion will have no effect on the peregrine falcon, bald eagle, or Mexican Spotted Owl." 109-1

The Biological Assessment report includes a response in Section III Consultation To Date, which was received from Robert G. Valentine, Director of the Utah Division of Wildlife Resources. This response states "Impacts to wildlife from this project as it is described should be minimal. The adjacent area is already heavily disturbed by the adjacent mining operations. The geomorphology of this area is steep and rocky, adding to the lack of suitable habitat for most wildlife species."

The Biological Assessment report also includes a response, in Section III Consultation To Date, from Robert D. Williams, Assistant Field Supervisor for the U.S. Fish and Wildlife Service(USFWS). Mr. Williams stated, "The U.S. Fish and Wildlife Service advises that no listed threatened or endangered species are known to occur on the project site."

As part of its biological assessment, the USFS searched the Utah Natural Heritage Program's Sensitive Species Database for occurrences of special status species that may occur within the proposed expansion area. The Biological Assessment report states, "The results of this search indicated that the database does not contain any information regarding special status species for the proposed expansion area."

109.3 Existing soil resources.

Response:

Existing soil resources are discussed in Section R647-4-106.5 of this NOI. For the reasons previously stated, no topsoil will be salvaged or stored unless it is considered practical.

109.4 Slope stability, erosion control, air quality.

Response:

The Operator conducted an investigation of the slope stability of the existing quarry in November 1997. A copy of the report entitled "Initial Evaluation Highwall Slope Stability Hank Allen Quarry" prepared by Dr. Ben L. Seegmiller of Salt Lake City, Utah is included in of Appendix No. 15 of this NOI.

Regarding slope stability, the report concluded:

- Slope undercutting discontinuities were not found.
- Rock mass strength in the limestone is very high.
- Rock mass strength in the shales is moderate to low.
- Groundwater pressurization is probably absent.
- Slope angles of 63.4 degrees (2:1) may be stable in limestone.
- Slope angles of 45 degrees (1:1) may be stable in shale.

Based upon the results from this initial study, the operator designed the slope angles of the quarry high-walls to be 63.4 degrees (2:1) in limestone and 45 degrees (1:1) in shale. All end-walls, regardless of the material were designed to be 45 degrees (1:1).

The operator contracted an additional highwall slope stability investigation in September 2001. A copy of the report entitled "Highwall Stability Evaluation, Ultimate Pit Slope Angles, Hank Allen Quarry - Leamington Plant, Central and Northeast Block Pits, Juab and Millard Counties, Utah" prepared by Seegmiller International, is included in Appendix No. 16 of this NOI.

The report makes the following recommendations:

- The Central Pit South Slope should be constructed with three step-outs (at 5,800-, 5,580-, and 5,400- feet) to mitigate safety concerns
- Interramp slope angles of 0.5:1 (63.4°) may be stable in limestone (L3 & L4)if blast damage reduction can be implemented and rockfall prevention is successful.
- Wheeler Shale (S4) may be stable with 1:1 (45°) slopes, and Chisolm Formation (S1, S2) may be stable with 2:1 (26.6°) slopes.

recognizes that there still exists a need to provide further slope stability investigations and ongoing testing will be necessary to prove these slope angles to be stable. The operator will commit to perform the additional testing as outlined in the recommendations made in Dr. Seegmiller's report. Testing should begin by the summer of 2002.

The pit has been designed largely according to the recommendations detailed in the highwall stability investigation. Step-out benches are planned at the 5,800-, 5,500-, and 5,300- foot elevations. The lowest step-out bench is 100 feet lower than what is recommended in the Seegmiller International report, but this bench is not planned for to be completed until at least 2025. The precise location of this lowest step-out bench may be adjusted pending results of future analyses. All pit design changes (if necessary) will be filed with the Division. Results from these studies will allow for additional analysis of slope stability and will be part of an ongoing incorporated into pit design planning performed by the operatorsystem. All reports, results, and pit design changes (if necessary), will be filed with the Division.

The Operator will use appropriate measures, such as fabric fences, check dams, etc., to control erosion. The Operator presently uses a water truck and a sprinkler system to control fugitive dust emissions from access and haul roads in the Quarry. The facility operates under an approved Title V Operating Permit (#2300015002) issued by the Utah Division of Air Quality.

The Operator limits access to the Plant and Quarry operations for

public safety. The Operator has marked the boundary of the Present Disturbance Limit to make it more visible to the public. The operator will also post signs along the perimeter of the Proposed Permit Boundary to advise the public of the Quarry operations.

109.5 Proposed mitigation of impacts.

Response:

No additional mitigation is proposed.

R647-4-110. Reclamation Plan.

110.1 Current land use and proposed post-mining land use.

Response:

The current land use for the Plant and Quarry areas within the Present Disturbance Limit is industrial/commercial. Specifically, the current land use is mining for the area included in the existing Quarry operations and is manufacturing for the area included in the existing Plant operations. The current land uses for lands outside of the Present Disturbance Limit, but within the Proposed Permit Boundary is rangeland, which includes livestock grazing, and use by wildlife.

The proposed post-mining land uses for all disturbed lands are rangeland, which includes livestock grazing and use by wildlife.

110.2 Manner and extent of reclamation.

Response:

ROADS

All roads except for the loop that extends north from Highway 132 to the railroad (the North road - 1.2 acres) and a road that extends south from Highway 132 to the Quarry (the South road - 4 acres) will be removed, ripped and reclaimed. These short road segments will be left for property access after operations cease.

HIGHWALLS

During the process of mining, when a highwall or end wall has been constructed it is dressed and stabilized by dragging a heavy chain across the face to remove any loose debris. A three (3) foot high berm is constructed on the edge of the bench below the rock wall to catch and contain any loose material. Once a highwall or end wall has been stabilized it will not be disturbed any further. Final standing highwalls and end walls will be left to provide potential habitat and cover for raptors and other wildlife species. Highwalls in limestone will not exceed slopes of 2V:1H, highwalls in S4 shale will not exceed slopes of 1H:1V, and highwalls in S1 and S2 shales will not exceed slopes of 2H:21V.

PONDS & DRAINAGES

All surface water diversion structures and sediment ponds shall be removed and the areas reclaimed. Pond embankments that were constructed will be removed to allow natural drainage systems to be re-established. Pond #1 which is located in the quarry will be filled with waste rock to the level of the final pit floor.

PIT FLOOR

Although previously approved submittals of this NOI specifically mentioned that no efforts would be made to revegetate the floor of the pit, the operator will attempt to revegetate a portion of the pit floor as part of reclamation. The area to be revegetated will be at least equal to the increase in acreage between the previously approved and proposed pit floor areas. Thus, since the previously approved pit floor was approved to reach approximately 46 acres without requiring revegetation, if the pit floor reaches its maximum area of 114 acres, the operator will attempt to revegetate a total of 68 acres of the pit floor. The areas selected for revegetation will be those considered to be most economical to revegetate, have the greatest chances for success, and have the lowest potential to exacerbate sediment runoff. Prior to revegetation, crushed rock on the pit floor will be amended with organic material, roughened, and revegetated with a seed mixture as shown in Table 4-110.1 or approved by the Division at the time of seeding.

WASTE ROCK STORAGE AREAS

The proposed waste rock stockpile will be constructed to be a stable slope of 1.5H:1Vapproximately 30 degrees. and will cover 29.0 acres. Runoff and erosion will be managed by surface roughening, mulching, and revegetation. Prior to revegetation, this area will be covered by fine-grained soil material obtained from the storage stockpile area located just north of the waste rock stockpile. Soil amendments may be added in order to increase the organic content of the soil and thus improve revegetative success. The waste rock pileIt will be revegetated by seeding with a seed mixture as shown in Table 4-110.1 or approved by the Division at the time of seeding.

Approximately 2.75 million cubic yards of waste rock will be generated while mining the Southwest Pit. For the next several years of operation, approximately 85,000 cubic yards of additional waste rock will be stockpiled at this location annually. Eventually, additional storage locations will be required, which will be submitted for approval in updated versions of this NOI.

PowerSieve uses normal photographs of the blasted rock that are digitally scanned to determine the distribution of rock fragment sizes. To determine the size distribution of the rock in the photographs, it is necessary to have a reference scale. In the field tests, a basketball, which is approximately 32 centimeters in diameter, is used as a reference scale. Using the reference scale, it is possible to use the software to measure the diameter of the rock fragments in the photographs.

After the photographs are digitized, the software plots graphs showing the distribution of the rock fragment sizes for limestone and for shale. The graphs show the X-axis as the size of the sieve in meters and the Y-axis as the percentage passing that size of sieve. The combined results of the analyses performed for all shale photographs taken at the Quarry are shown on the graph in Figure 4-110-2-1 of this NOI. The combined results of the analyses for all limestone photographs taken at the Quarry are shown on the graph in Figure 4-110-2-2. These graphs are included in this section of the NOI.

Both the limestone and shale cumulative size distribution at the Quarry exhibit a narrow size range from powder size up to a larger size of 0.20 meters (approximately 8 inches). Using the current blasting

design produces, a run-of-mine rock size distribution where more than 50 percent of the limestone and shale is less than 0.05 meters in size (approximately 2 inches and less). This analysis provides data that shows the particle size in the waste rock storage areas will contain sufficient fines to allow re-vegetation and successful growth of vegetation to reclaim these areas.

110.3 Surface facilities to be left as part of postmining land use.

Response:

All features such as buildings, roads (except for two discussed above), pads, or other structures will be removed and the areas reclaimed during the final reclamation process.

110.4 Description of the treatment, location and disposition of any deleterious or acid-forming materials generated and left on-site, including a map showing the location of such materials upon the completion of reclamation.

Response:

There are no deleterious or acid-forming materials known to be present on the site.

- 110.5 Planting program as best calculated to re-vegetate the disturbed area.
 - 110.5.11 Plans shall include, at a minimum, grading and/or stabilization procedures, topsoil replacement, seedbed preparation, seed mixture(s) and rate(s), and timing of seeding (fall seeding is preferred timing).

Response:

Disturbed lands, where required, will be ripped to reduce compaction, rough graded to re-establish contours and drainage and final graded to slopes suitable for use of mobile equipment, as may be required, for the preparation of seedbeds and re-vegetation.

Appropriate stabilization methods, including but not limited to, rock, straw or hay bale check dams, geotextile fabric fences, berms, etc. will be used to control erosion and stabilize slopes and disturbed lands.

Disturbed areas, except for barren rock highwalls, and portions of the pit floor will be graded and stabilized, and seeded in either the fall (preferred) or spring. Prior to seeding, the Operator will contact the Division to confirm the recommended seed mixture. It is anticipated that a seed mix similar to the one shown in Table 4-110-1 of this NOI will be used.

SOIL FERTILITY

Reconstructed soil materials will be tested for fertility prior to commencement of re-vegetation operations. Laboratory results will be used to calculate the amounts and types of amendments needed to provide a suitable rangeland plant community environment. Based on laboratory analysis, the need for fertilizers and other amendments will be made. When soil supplements, fertilizers or other amendments are required or desirable, they will be applied properly per the manufacturer's specifications.

REVEGETATION SPECIES

Reclamation of the Quarry will be accomplished by planting a diversified mixture of grasses, forbs and shrubs approved by the Division. The plant community that is established by this seed mixture will support the postmining land use of rangeland, which includes livestock grazing and use by wildlife. The seed mixture shown on Table 4-110-1, or as recommended by the Division at the time of reclamation, is proposed for use for permanent re-vegetation of lands disturbed by mining. The seed mixture contains a variety of species, including drought resistant varieties that grow in the region of the Quarry and are adapted to the environmental conditions that may be found at or near the Quarry site.

The species contained in this permanent re-vegetation seed mixture may be substituted, or their percent composition, varied from year-to-year based on commercial availability and actual site performance. However, the Division will be consulted prior to such substitutions being made. Actual purity and germination values for specific seed lots will be used in formulating bulk rates for each species contained in the seed mixture each year.

SEEDING & PLANTING METHODS

Broadcasting will be the preferred method used for planting seed. Broadcasting will be accomplished by both ground and aerial means, depending on the steepness and safe accessibility of the ground surface. When properly conducted, broadcast seeding is usually superior to drill seeding for establishment of native species seed mixtures. The main advantage realized by broadcast seeding in reclaiming rangeland is that it distributes seed more evenly across the ground surface. This limits the competition between seedlings and young plants. Broadcasting also maximizes the nutrient and water availability for seedlings and young plants.

Table 4-110-1	COMPANY - LEAMINGTON QUARRY, UTAH T REVEGETATION SEED MIXTURE
Tab	ASH GROVE CEMENT COMPANY PERMANENT REVEGET

SCIENTIFIC NAME	COMMON NAME	SEEDIN	SEEDING RATE
		TTL PLS LBS	PLS LBS/ACRE
Penstemon eatonii	Eaton's penstemon (Firecracker)	0.5	0.50
Penstemon palmeri	Palmer Penstemon	0.5	0.50
Agropyron intermedium	Intermediate wheatgrass	2.0	2.0
Dactylis glomerata var. Piaute	Piaute Orchardgrass (drought resistant variety)	1.0	1.0
Kochia prostrata	Forage Kochia (subshrub)	0.5	0.5
Chrysothamnus nauseosus	Rubber Rabbitbrush	0.5	0.5
Melilotus officinalis	Yellow Sweetclover	1.0	1.0
Medicago sativa var. Ladak	Alfalfa	1.5	1.5
Agropyron cristatum var. Hycrest	Crested wheatgrass	1.0	1.0
Leymus cinereus	Basin Wild Rye	2.0	2.0
Artemisia tridentate wyomingensis	Wyoming Big Sage	0.1	0.1
Achnatherum hymennoides	Indian ricegrass	2.0	2.0
TOTAL		12.6	12.6

Characteristically, this results in an optimal expression of the diversity contained in the seed mixture and fosters improved plant growth. In order to realize optimum expression of the variety of species contained in the seed mixture, broadcast seeding will be performed as soon as possible after the seedbed has been prepared.

Seed mixtures will be distributed as evenly as possible over the area being re-vegetated. Drill seeding may be employed when slopes are less than 40 percent and where soils are not excessively rocky. Broadcast seeding may be performed on all slopes and on all soils regardless of percentage of rock composition. Broadcasters may be human-powered or machine-powered as long as they are properly equipped and are capable of distributing seed evenly at the required rates. Broadcasting will not be performed when surface winds prevent the even distribution of seed. Broadcasting by hand will be used in certain areas where equipment cannot be used but are accessible safely by foot.

PLANTING PERIODS

The amount and timing of precipitation impacts the successful germination and establishment of re-vegetation plantings. Native western rangeland plants have developed various adaptations for ensuring their survival in low moisture conditions. Seed mixtures will be planted in either the fall or spring of each year at the discretion of Leamington Quarry personnel.

Germination in many western plants is triggered by certain environmental or climatic conditions. These conditions may not occur every year. As a result, full germination of the seed, contained in a diverse native plant seed mixture, on arid and semi-arid land may take one or more years to occur. Western native plant seed may remain viable for many years (5+ years). It is important to allow adequate time for seed mixture germination and establishment before deciding that re-vegetation is a failure or is substandard and initiating interseedings. Patience must be exercised in determining whether or not a specific re-vegetation seeding is a success or failure. Premature application of additional seed is a frequent practice that can adversely impact biologic diversity in western rangeland reclamation.

Seeding operations will be performed during the normal seeding period for the types of species being planted. When cool season species comprise the majority of the seed mixture, planting will normally be performed in the fall after September 15th, or in the spring prior to May 1st.

When warm season species comprise the majority of the seed mixture, planting operations may be conducted during the same periods as cool season species, except that spring seeding may be extended through May 30th. Seeding activities will be conducted as weather and soil conditions permit. Seeding will not be performed when there are more than two inches of snow on the ground.

SEED QUALITY

Certified, weed-free seed will be procured whenever possible. Seed used in permanent re-vegetation operations will be site-adapted, improved varieties and cultivars of native grasses, forbs and shrubs. Seed sources that are from the same general locality will be used whenever possible. Seed from more distant sources may be used as dictated by availability, with care being taken to match climatic zones to the extent necessary and possible.

SEEDBED PREPARATION

Seedbeds will be prepared to facilitate seedling germination and establishment. Seedbeds will be left in a rough surface condition whenever possible. Areas will be seeded as soon as possible after completion of soil reconstruction. Physical soil manipulation and re-vegetation operations will be performed on the contour, to the fullest extent possible, to minimize potential surface erosion. Specific cultural practices that promote the establishment and survival of seeded forbs and shrubs will be employed where practicable, subject to the approval of the Division.

SEED MIXTURE APPLICATION RATE

Seed mixtures will be applied at the approximate rate of 20 pure live seeds ("PLS") per square foot. Application rates may be varied with the Division's approval as the germination, establishment and growth of previous seedings are observed and evaluated. When the bulk-seeding rate for a sub-mixture is very low (i.e., less than 10 pounds/acre), an extender may be added to aid in seed mixture distribution and coverage. A commonly used extender is cracked corn, but other materials may be used providing they are environmentally benign. When extenders are used, they will be thoroughly mixed with the seed prior to commencement of seeding operations.

ALTERNATIVE WOODY PLANT ESTABLISHMENT

Bare root, tubling, or containerized native shrub and tree species may be hand planted in selected areas that may support the establishment of these species. Plant establishment may be enhanced with the use of slow-release fertilizer tabs, plant protectors and "Terrasorb" or "DRIWATER".

MULCHING

Mulching involves the application of plant residues, compost manure, or other suitable materials to the soil surface. The purpose of mulching is to conserve moisture, increase organic matter, prevent surface compaction or soil crusting, and control weeds. Mulching aids in establishing plant cover and reduced erosion and runoff, thereby protecting the quality of surface runoff. Mulching may be necessary where there is a wind or water erosion hazard, on soils with low infiltration rates or low organic matter present, on critical areas, on sites where annual precipitation is less than 12 inches, or on slopes that are greater than 3h:1v.

The preferred method to increase organic matter, when soils data indicates that it is low, will be to apply composted manure. Composted manure will be applied at the rate of five (5) tons per acre for areas that receive a minimum of six (6) inches of topsoil and ten (10) tons per acre for areas that receive less than six (6) inches of topsoil or areas where substitute topsoil materials are used. Composted manure would be applied to the surface and ripped just prior to seeding.

Hay and straw mulches may be put on areas with extreme erosion potential and shall be applied at the rate of approximately 2 tons per acre. Mulch may be spread by hand or mechanical methods. Mulch materials will be evenly and uniformly distributed over the site to be treated. All mulching materials will be certified, weed-free. To realize maximum effectiveness, mulches will be crimped, netted or tackified using standard accepted practices. Whenever possible, anchoring will be performed at right angles to prevailing winds or on the contour. Broadcasting or drilling of seed will be performed immediately following mulch applications. When seed is drilled, operations will follow crimped rows to the extent this is practicable.

SURFACE ROUGHENING/WATER HARVESTING

Ripping, land imprinting, contour furrowing or a similar surface roughening procedure may be performed to reduce surface water runoff and increase moisture harvesting. Moisture harvesting associated with surface roughening can be expected to improve soil moisture content and stimulate plant growth and development.

MONITORING AND INTERSEEDING

Re-vegetated areas will be monitored for adequate germination and establishment. Vegetation stand establishment and development will be observed annually in the later part of the growing season following seeding and may continue for several years thereafter. Stand germination and establishment may take several growing seasons before full expression of the seed mixture is realized. Many xeric plant species will not germinate until specific environmental conditions occur. Seed can remain dormant and viable for such species for many years. For this reason full expression of seeded materials may take several years to occur.

110.5.12 Where there is no original protective cover, an alternate practical procedure must be proposed to minimize or control erosion or siltation.

Response:

In some areas where there is no original protective cover, native species in tublings may be hand planted in selected areas that may be conducive to growth. These tublings will include fertilizer, stake with plastic protector to lessen rodent damage and a packaged water, cellulose gum and alum mixture, such as "Terrasorb" or "DRIWATER", to provide water and to aid in survivability.

110.6 Operator's Statement

Response:

The Operator will conduct reclamation in accordance with these rules.

R647-4-111. Reclamation Practices.

During reclamation, the Operator shall conform to the following practices, unless the Division grants a variance in writing:

- 111.1 Public Safety and Welfare The operator shall minimize hazards to the public safety and welfare following completion of operations. Methods to minimize hazards shall include but not be limited to:
 - 111.1.11. The permanent sealing of shafts and tunnels;

Response:

To the best knowledge of the Operator there are no shafts or tunnels on the property being mined. If any tunnels or shafts are encountered, the Operator shall permanently seal them as required by the Division.

1.12. The disposal of trash, scrap metal and wood, buildings, extraneous debris, and other materials incident to mining;

Response:

The Operator shall conform to environmentally protective methods for the proper disposal of trash, scrap metal and wood, buildings, extraneous debris, and other materials incident to mining.

1.13. The plugging of drill, core, or other exploratory holes as set forth in Rule R647-4-108;

Response:

The Operator shall plug all drill, core, or other exploratory holes as set forth in Rule R647-4-108.

1.14. The posting of appropriate warning signs in locations where public access to operations is readily available;

Response:

The Operator shall post appropriate, legible warning signs in locations where public access to operations is readily available and in the immediate vicinity of reclamation operations.

1.15. The construction of berms, fences and/or barriers above highwalls or other excavations when required by the Division.

Response:

The Operator currently dresses the highwalls by dragging a heavy chain across the face to remove any loose debris. A three (3) foot high berm is constructed on the edge of the bench below the highwall to catch and contain any loose material from the highwall. The Operator shall construct berms, fences and/or barriers above highwalls or other excavations when required by the Division. The Operator shall install a berm or fence above the highwall in locations where public access to the pits are readily available. Berms or fences will not be built in areas of difficult access such as in areas of steep natural slopes. In these locations, access is extremely difficult, and the frequency of human traffic is negligible. The hazards associated with installing protective measures would far outweigh their safety benefits.

111.2 Drainages - If natural channels have been affected by mining operations, then reclamation must be performed such that the channels will be left in a stable condition with respect to actual and reasonably expected water flow so as to avoid or minimize future damage to the hydrologic system.

Response:

If natural channels are affected by mining operations, the Operator shall perform reclamation in a manner such that the channels will be left in a stable condition with respect to actual and reasonably expected water flow, so as to avoid or minimize future damage to the hydrologic system. The location of reclamations channels can be seen on the map in Appendix 8. A typical cross-section of the channels can also be seen in Appendix 8. Table 4-111-2-1 contains the channel configurations and the maximum capacity of the reclamation channels. All reclamations channels can handle the 100-year 6-hour storm event of 2.1 inches. Reclamation channels have been designed to approximate the natural channels in the area.

111.3. Erosion Control - Reclamation shall be conducted in a manner such that sediment from disturbed areas is adequately controlled. The degree of erosion control shall be appropriate for the site-specific and regional conditions of topography, soil, drainage, water quality or other characteristics.

Response:

The Operator shall conduct reclamation in a manner such that sediment from disturbed areas is adequately controlled. The degree of erosion control shall be appropriate for the site-specific and regional conditions of topography, soil, drainage, water quality or

other characteristics.

111-2

Table 4-111-2-1

ASH GROVE CEMENT COMPANY - LEAMINGTON QUARRY, UTAH RECLAMATION CHANNEL SUMMARY

Channel	Bottom Width (ft)	Side Slope (H:V)	Depth (ft)	Design Flow Rate (cfs)	Maximum Channel Capacity (cfs)	Erosion Control Method
RC-1	18	5:1	2.0	328.0	457.5	Erosion control Mat*
RC-2	30	5:1	1.0	25.3	135.5	None
RC-3	0	3:1	1.5	9.2	32.3	None
RC-4	20	5:1	1.0	109.1	214.7	Erosion control Mat*
SWALE-1	5	10:1	1.5	25.3	95.9	None

Notes:

*Erosion Control Mat denotes a three-dimensional vegetation reinforcement mat such as Tensar TM-3000 or equal. Using this product allows the channel to be reinforced and still appear like an undisturbed natural channel. Channels reinforced using this method can withstand flow velocities up to 14 fps before vegetation is established and 20 fps after vegetation is established according to the manufacturer. In the worst case condition the flow velocity should not exceed 12.7 fps for the design storm event.

The design storm event is the 100-year 6-hour storm event, which is 2.1 inches of rain in a 6 hour period.

111.4. Deleterious Materials - All deleterious or potentially deleterious material shall be safely removed from the site or left in an isolated or neutralized condition such that adverse environmental effects are eliminated or controlled.

Response:

The deleterious materials encountered during reclamation are expected to be small amounts of materials identified in Section 107.1.12. They will be handled in an environmentally protective manner as specified in Section 107.1.12. There are no deleterious or potentially deleterious materials on the site. However, if any such material is found, the Operator shall safely remove all deleterious or potentially deleterious material from the site or leave it in an isolated or neutralized condition, such that adverse environmental effects are eliminated or controlled.

111.5. Land Use - Operator shall leave the on-site area in a condition capable of supporting the postmining land use.

Response:

The Operator shall leave the on-site area in a condition that is capable of supporting the proposed post-mining land use of rangeland.

111.6. Slopes - Waste piles, spoil piles and fills shall be regraded to a stable configuration and shall be sloped to minimize safety hazards and erosion while providing for successful revegetation.

Response:

The Operator shall re-grade all waste piles, spoil piles and fills to a stable configuration. Such piles and fills shall be sloped to minimize safety hazards and erosion, while providing for successful revegetation. The out-of-pit waste rock disposal area will be constructed to a maximum slope of approximately 30 degrees 1.5 horizontal to 1 vertical.

111.7. Highwalls - In surface mining and in open cuts for pads or roadways, highwalls shall be reclaimed and stabilized by backfilling against them or by cutting the wall back to achieve a slope angle of 45 degrees or less.

Response:

The Operator has previously obtained a variance from the Division to allow highwalls of approximately 63 degrees (2v:1h) in limestone in the central area of the Quarry. The Operator is requesting a similar variance in this NOI to allow highwalls of 63

degrees (2v:1h) in limestone when mining is extended into the Northeast reserve block and the Southwest expansion area of the Quarry. The Northeast reserve block and the Southwest expansion area are shown on the Proposed Life-Of-Quarry Disturbance Limit Map in Appendix No. 9 of this NOI. When mining in shale the Operator will mine to achieve a highwall slope of 45 degrees (1v:1h) or less.

111.8. Roads and Pads - On-site roads and pads shall be reclaimed when they are no longer needed for operations. When a road or pad is to be turned over to the property owner or managing agency for continuing use, the operator shall turn over the property with adequate surface drainage structures and in a condition suitable for continued use.

Response:

The Operator shall reclaim all on-site roads and pads, except for two short road segments described below.

One road segment (the North Road), which extends from the north side of Highway 132 approximately 700 feet to the railroad, will not be reclaimed. The North Road will be left in place for use by the Division for post-mining reclamation inspection of the property, use by property owners for access to the Leamington irrigation canal and to private property located north and northeast of property owned by the Operator. The Operator (the property owner) will also use this road for access to their property adjacent to the railroad.

The second road segment (the South Road), which extends from the south side of Highway 132, approximately 0.9 mile to the south towards the mined pit, will be not be reclaimed. The South Road will be left in place for use by the Division for post-mining reclamation inspection of the property and by the Operator (the property owner) for access to their property.

The two roads to remain will be dirt roads no more than 12 feet wide. Paving materials will be removed or ground up in place prior to ripping the soil.

111.9. Dams and Impoundments - Water impounding structures shall be reclaimed so as to be self-draining and mechanically stable unless shown to have sound hydrologic design and to be beneficial to the postmining land use.

Response:

- All water impounding structures will be reclaimed so as to be self-draining and mechanically stable.
- 111.10. Trenches and Pits Trenches and small pits shall be reclaimed.

Response:

The Operator shall reclaim all trenches and small pits.

111.11. Structures and Equipment - Structures, rail lines, utility connections, equipment and debris shall be buried or removed.

Response:

The Operator shall bury or remove all structures, rail lines, utility connections, equipment and debris.

111.12. Topsoil Redistribution - After removal of structures and completion of final grading, any available soil materials shall be redistributed on a stable surface, so as to minimize erosion, prevent undue compaction and promote re-vegetation.

Response:

For the reasons previously explained in Sections R647-4-106.6 and 107.5 of this NOI, the Operator does not propose to remove and store topsoil materials. However, if any topsoil materials are removed and stored the Operator shall, after removal of structures and final grading, redistribute any available soil materials on a stable surface, so as to minimize erosion, prevent undue compaction and promote re-vegetation.

111.13. Revegetation - The species seeded shall include adaptable perennial species that will grow on the site, provide basic soil and watershed protection, and support the postmining land use.

Response:

The species seeded by the Operator shall include adaptable perennial species that will grow on the site, provide basic soil and watershed protection, and support the postmining land use.

Re-vegetation shall be considered accomplished when:

13.11. The re-vegetation has achieved 70 percent of the premining vegetative ground cover. If the premining vegetative ground cover is unknown, the ground cover of an adjacent undisturbed area that is representative of the premining ground cover will be used as a standard. Also, the vegetation has survived three growing seasons following the last seeding, fertilization or irrigation, unless such practices are to continue as part of the postmining land use;

Response:

The Natural Resources Conservation Service prepared a Soil and Vegetation Survey of certain lands included within the Proposed Permit Boundary. A copy of this Soil and Vegetation Survey is included in Appendix No. 11 of this NOI. Mr. Ken Sevy, Soil Conservationist, stated the Survey provided "...the present estimated percents of vegetation on the site". This estimate represents pre-mining vegetative ground cover in the area of the Quarry and Plant. The Operator proposes this estimate be used to determine pre-mining vegetative ground cover under Section R647-4-111.13.11; or

13.12. The Division determines that the re-vegetation work has been satisfactorily completed within practical limits.

R647-4-112. Variance.

- 1. The operator may request a variance from Rule R647-4-107, 108, or 111, by submitting the following information which will be considered by the Division on a site-specific basis:
- 1.11. The rule(s) as to which a variance is requested;

Response:

Ash Grove requests a variance from the following Rules: Rule R647-4-111.7 Highwalls, and Rule R647-4-111.8 Roads and Pads

1.12. The variance requested and a description of the area that would be affected by the variance;

Response:

Rule R647-4-111.7 Highwalls

A variance request from Rule 647-4-111.7 is made by the Operator to allow additional mining of limestone highwall slopes of 2 vertical to 1 horizontal (approximately 63 degrees) in the Central, Northeast, and Southwest reserve blocks as discussed in Section 105.3.11 and 105.3.14 of this NOI. The locations of these slopes are shown on Drawing 4-106-1 included in Section 4-106 of this NOI and on the Reclamation Activities & Treatment Map included in Appendix No. 6 of this NOI.

A variance from Rule 647-4-111.7 was previously granted to the Operator by the Division, by letter dated July 23, 1996. This variance was to allow the Operator to construct highwall slopes of 2 vertical to 1 horizontal (approximately 63 degrees). That variance was described as being applicable to the "current quarry area" as defined on maps included with Ash Grove's letter dated April 4, 1996. At the time the Operator requested this variance, mining was being conducted in what is now identified as the Central reserve block.

A separate variance request from Rule 647-4-111.7 is made by the Operator in this NOI to allow mining of highwall slopes of 2 vertical to 1 horizontal (approximately 63 degrees) in the Northeast reserve block as discussed in Section 105.3.11 and 105.3.14 of this NOI. The location of these slopes are shown on Drawings 4-106-11 and 4-106-12 included in Section 4-106 of this NOI and on the Reclamation Activities & Treatment Map included in Appendix No. 6 of this NOI.

While at this time the operator is requesting this variance additional testing as outlined in Dr. Seegmillers report and as discussed in Section 109.4 of this NOI will be ongoing. Results from this study will be part of a continuing pit design planning system and all results will be shared with the Division.

At a later date, the Operator intends to request a similar variance in the Southwest pit future expansion area, as shown on the Proposed Life-Of-Quarry Disturbance Limit Map in Appendix No. 9 of this NOI.

Rule R647-4-111.8 Roads and Pads

A variance request from Rule R647-4-111.8 is requested by the Operator in this NOI to allow two short road segments identified as the North road and the South road to be partially reclaimed after operations are completed. Pavement would be removed from the roads, which would be reduced to a width of approximately 12 feet. These road segments are described in Sections R647-4-105.3.12, 105.3.14, 110.3 and 111.8 of this NOI and their locations shown on the Reclamation Activities & Treatment Map included in Appendix No. 6 of this NOI.

A variance request from Rule R647-4-111.8 is requested by the Operator in this NOI to allow two short road segments identified as the North road and the South road to not be reclaimed and remain in-place after operations are completed. These roads segments are described in Sections R647-4-105.3.12, 105.3.14, 110.3 and 111.8 of this NOI and their locations shown on the Reclamation Activities & Treatment Map included in Appendix No. 6 of this NOI.

1.13. Justification for the variance;

Response:

Rule R647-4-111.7 Highwalls

The variance from Rule R647-4-111.7 is requested to allow the Operator to continue the same method of operation it now conducts as mining progresses in the Central and Northeast reserve blocks as well as the Southwest pit expansion area. Cutting the highwall back to achieve a slope of 45 degrees or less would disturb more of the shale units, which are not useful materials. This would result in the disturbance of additional land and create additional waste rock to be disposed of.

An identical variance to this rule was previously granted to the Operator by the Division in a letter dated July 23, 1996. This variance allowed the Operator to construct highwall slopes of 2 vertical to 1 horizontal (approximately 63 degrees). That variance was described as being applicable to limestone slopes in the "current quarry area" as defined on maps included with Ash Grove's letter dated April 4, 1996. At the time the Operator requested this variance, mining was being conducted in what is now identified as the Central reserve block.

The current variance request is justified both by the historic stability of the highwalls in the central pit and by extensive rock slope stability analyses. The 63 degree highwall slopes, as previously approved by the Division, in the central area of the Quarry have maintained stable slopes and have not caused any unstable or unsafe conditions in the mining operation. This stability is also demonstrated by the highwalls of the old abandoned Chaffin Quarries on the property. These highwalls are nearly vertical and have stood without any failure since the early 1900's.

Additionally, Dr. Ben L. Seegmiller, a consulting mining geotechnical engineer, has examined the slopes in the Quarry and commented that slope angles of 63.4 degrees (2:1) are likely to be stable in limestone. Dr Seegmiller produced two reports on rock slope stability for this site, which are included as Appendices Nos. 15 and 16. In his detailed slope stability analysis, he collected and analyzed core drilling and logging data, performed field and laboratory strength tests, and completed detailed slope stability analyses for the slopes at the Central and Northeast Blocks. He concluded that in the Northeast Block, limestone slopes would maintain a factor of safety against rotational shear failure of at least 1.3 if they were left at 2V:1H (63.4°). He concluded that shale slopes would maintain the same factor of safety if left at 1H:1V (45°) in the S4 shale and 2H:1V (26.6°) in the S1 and S2 shales.

He also concluded that the limestone highwalls in the Central Pit South Slope would maintain a factor of safety of 1.2 to 1.3 against rotational shear failure if left at 2V:1H (63.4°) slopes provided that adequate benches and ramps are left at various levels in the pit. He recommended three 75-foot wide ramps at the 5,800-, 5,580-, and 5,400-foot elevations, and 25-foot catch benches every 60 vertical feet down the highwall.

The operator has chosen to construct the south slope of the central pit with 60-foot tall benches separated by 30-foot wide ramps with 75-foot wide ramps at the 5,800-, 5,580-, and 5,300-foot elevations. This configuration conforms to the design in the Seegmiller report, except that ramps are conservatively designed slightly wider than recommended and the location of the lowest step-out is 100 feet lower than recommended. Since the majority of the Central Reserve Block is currently excavated to 5,700 feet, observations and data can be collected for several years in order to determine whether lowering the location of the lowest step-out bench is justified. The operator will continue to monitor slope stability within the pit and will modify its design if necessary. All pit design changes will be filed with the Division.

The variance from Rule R647-4-111.7 is requested to allow the Operator to continue the same method of operation it now conducts as mining progresses from the Central reserve block into the Northeast reserve block and later into the Southwest pit expansion area. Cutting the highwall back to achieve a highwall slope of 45 degrees or less would disturb more of the shale units, all of which are not useful materials. This would result in the disturbance of additional land and create additional waste rock to be disposed.

The 63 degree highwall slopes, as previously approved by the Division, in the central area of the Quarry have maintained stable slopes and have not caused any unstable or unsafe conditions in the mining operation. The stability of steep slopes in the limestone units can be demonstrated by examining the highwalls of the old abandoned Chaffin Quarries on the property. These highwalls are nearly vertical and have stood without any failure since the early 1900's.

Additionally, Dr. Ben L. Seegmiller, a consulting mining geotechnical engineer, has examined the slopes in the Quarry and commented that slope angles of 63.4 degrees (2:1) may be stable in limestone. Dr Seegmiller produced two reports on rock slope stability for this site, which are included as Appendices Nos. 15 and 16. In his detailed slope stability analysis, he collected and analyzed core drilling and logging data, performed field and laboratory strength tests, and completed detailed slope stability analyses for the slopes at the Central and Northeast Blocks. He concluded that in the Northeast Block, limestone slopes would maintain a factor of safety against rotational shear failure of at least 1.3 if they were left at 2V:1H (63.4°). He concluded that shale slopes would maintain the same factor of safety if left at H:1V (°)

He also concluded that the limestone highwalls in the Central Pit South Slope would maintain a factor of safety of 1.2 to 1.3 against rotational shear failure if left at 2V:1H (63.4°) slopes provided that adequate benches and ramps are left at various levels in the pit. He recommended three 75-foot wide ramps at the 5,800-, 5,580-, and 5,400-foot elevations, and 25-foot eatch benches every 60 vertical feet down the highwall.

The operator has chosen to construct the south slope of the central pit with 60-foot tall highwalls separated by 30-foot wide ramps. This configuration has historically proven stable for other areas of the operation, and will allow for maximum resource recovery. The operator will continue to monitor slope stability within the pit and will modify its design if necessary. He further commented that for the limestones, a maximum slope height of 840

vertical feet would have a safety factor, against rotational shear failure, of approximately 1.70. His conclusion was that the highwall and low wall in limestone should be quite safe concerning rotational shear. Dr. Seegmiller commented that for the highwall and low wall, which are fully within the strong limestones, the overall angle of 63.4 degrees (2:1) should be acceptable for slopes up to 840 feet high, based on available stability data.

Additional tests were recommended to confirm the initial findings. The operator plans to start these tests no later than the summer of 2002. Results from these tests will be implemented into the current pit design and changes will be made if the findings so warrant. All test results will be shared with the Division and changes to the current pit design will only be made with the Divisions approval. The report entitled "Initial Evaluation Highwall Slope Stability Hank Allen Quarry" is included in Appendix No. 15 of this NOI.

Rule R647-4-111.8 Roads and Pads

The variance from Rule R647-4-111.7 is requested so that the Operator and adjacent landowners may access their properties after mining operations have been completed. By removing pavement and reducing the width of the roads, their condition will be such that they will become self-reclaimed unless maintained by the landowner(s).

The variance from Rule R647-4-111.7 is requested to allow the Operator the means to access property it owns in fee after mining operations have been completed. The variance also allows other landowners to continue to use the North road to access their property.

1.14. Alternate methods or measures to be utilized.

Response:

Rule R647-4-111.7 Highwalls

The alternative to the requested variance from Rule R647-4-111.7 would be re-design the mine plan and cut the highwall back to achieve a slope of 45 degrees or less. This would result in a greater area of land being disturbed, smaller recoverable limestone reserves and a larger volume of waste rock to be disposed. It is likely that such a slope configuration would make mining operations economically and environmentally unfeasible.

Rule R647-4-111.8 Roads and Pads

The alternative to the requested variance from Rule R647-4-111.8 would be to reclaim the two short road segments. However, this would eliminate access the property by the landowner and in the case of the North road, would cut off access by other landowners to their property.

2. A variance shall be granted if the alternative method or measure proposed will be consistent with the Act.

Response:

The Operator respectfully requests the Division approve the variances requested above. The Operator believes approval of the variance requested to Rule R647-4-111.7 to be consistent with the Act as evidenced by the Division previously granting a similar variance for the current central quarry area. The Operator also believes the other variance, as requested, is be consistent with the Act.

3. Any variance must be specifically approved by the Division in writing.

Response:

The Operator understands that any variance must be specifically approved by the Division in writing.

R647-4-113. Surety.

113.1. After receiving notification that the notice of intention has been approved, but prior to commencement of operations, the operator shall provide the reclamation surety to the Division.

Response:

The Operator, after receiving notification from the Division that this NOI has been approved, will adjust the current surety bond that is in place.

- 113.2. The Division will not require a separate surety when a reclamation surety in a form and amount acceptable to the Board is held by the Division of State Lands and Forestry, or an agency of the federal government.
- 113.3. As part of the review of the notice of intention, the Division shall determine the required surety amount based on site specific calculations reflecting the Division's cost to reclaim the site. An operator's estimate will be accepted if it is accurate and verifiable.

Response:

The Operator has performed site-specific calculations based on both RSMeans construction costs and site-specific cost estimates to determine the cost to reclaim the site and determine the surety amount. These calculations are included at the end of this section of the NOI and are summarized in Table 4-113-3-1. The cost for reclamation was calculated by first preparing an inventory of all structures located in the Plant and Quarry. This inventory included the dimensions and construction type of all existing structures. The location and identification of these structures are shown on the Surface Facilities - Plant and Surface Facilities - Quarry Maps included in Appendices No. 4 and No. 5 of this NOI.

The Proposed Life-Of-Quarry Disturbance Limit was determined by overlaying the limits of the pits, as modeled by MINEX mining software on a base map created in AutoCAD Map 2000 software. The areas needed for future disturbance were compared to the Present Disturbance Limit as shown on the black and whitecolor photo in Appendix No. 3 of this NOI. The disturbance limit was adjusted to include all areas presently disturbed; all areas needed for future disturbance; and a reasonable buffer around the disturbance areas. The acreage included in the resulting Proposed Life-Of-Quarry Disturbance Limit Map was determined by AutoCAD Map 2000 to be 669 increase from 669 acres to 731 acres. The acreage figure of 669 731 acres was used in determining re-vegetation and reclamation costs.

Note that since most of the pit floor will not be revegetated, an increase in its area can reduce the acreage of reclamation revegetation. The ultimate pit will cover 230 acres, of which 114 acres would be the pit floor. As stated on Section R647-4-110.2, attempts will be made to revegetate 68 acres of the pit floor (Note that the attached surety estimate includes 30 acres of pit floor revegetation, which is the current area of the pit floor. As the pit expands into the Northeast and Southwest Blocks, additional revegetation acreage will be added to the surety estimate). The North and South Access roads and the remaining Chaffin quarries (these areas also will not be revegetated) will cover a total of 4 acres. Thus, the final area of reclamation revegetation is estimated to total 565 acres. The Proposed Life-Of-Quarry Disturbance Limit Map is included in Appendix No. 9 of this NOI.

R.S. Means Heavy Construction Cost Data, 13th21st Annual Edition (19992007) was used to estimate the demolition, haulage, disposal, and re-vegetation costs of the reclaimed lands. Means CostWorks '99 interactive cost books software was used to calculate the reclamation surety estimate. A copy of this cost data was exported into an Excel spreadsheet. The cost data was escalated to 2012 dollars using escalation factors supplied by the Division. A copy of this spreadsheet entitled "Surety Estimate Using CostWorks 19992007 Construction Cost Data - Ash Grove Cement Company - Leamington Plant and Quarry" is included at the end of this Section of the NOI.

An estimated 669-731 acres is proposed to be disturbed over the life of the Quarry. The total estimated reclamation surety amount, including a 10% contingency and escalation for five (5) years at $\frac{3.273.20}{3.273.20}$ percent, is $\frac{4,372,057}{6,766,000}$. This puts the average cost per disturbed acre at $\frac{6,535.21}{9,255}$.

- 113.4. The operator shall submit a completed Reclamation Contract (FORM MR.-RC) with the required surety. The form and amount of the surety must be approved by the Board. Acceptable forms may include:
 - 4.11. Corporate surety bond;
 - 4.12. Federally-insured certificate of deposit payable to the State of Utah, Division of Oil, Gas and Mining;
 - 4.13. Cash:
 - 4.14. An irrevocable letter of credit issued by a bank organized to do business in the United States;
 - 4.15. Escrow accounts.
 - 4.16. In addition, the Board may accept a written self-bonding agreement in the case of operators showing sufficient financial strength.

Response:

A completed Reclamation Contract (FORM MR-RC) will be submitted by the Operator in the amount stated upon approval by the Division of the surety estimate. A copy of the Division's Form MR-RC (revised January 7, 1999) is included at the end of this section of the NOI.

- 113.5. Surety shall be required until such time as reclamation is deemed complete by the Division. The Division shall promptly conduct an inspection when notified by the operator that reclamation is complete. The full release of surety shall be evidence that the operator has reclaimed as required by the Act.
- 113.6. Adjustments or revisions made in the surety amount shall be in accordance with the terms and conditions outlined in the Reclamation Contract.

Table 4-113-3-1		
ASH GROVE CEMENT COMPANY - LEAMINGTON SURETY SUMMARY	N C	UARRY, UTAH
Reclamation Activities		
Cleanup, Removal, Demolition and/or Burial of Facilities and Structures	\$	1,074,985.71
Removal and Disposal of Hazardous Materials	\$	15,367.67
Backfilling, Grading and Contouring	\$	271,133.96
Ripping Pit Floors, Access Roads, and Slopes	\$	2,602,606.88
Drainage Reconstruction	\$	123,401.00
Mulching and Revegetation	ş	709,621.25
General Site Cleanup	\$	8,772.00
SUBTOTAL	\$	4,805,888.46
Administrative Costs		
Contigency (10%)	\$	480,588.85
Reclamation Supervision (10%)	Ş	480,588.85
Mob/Demob	\$	12,810.00
Escalation (Assume 3.2% apr)	\$	985,890.56
TOTAL	\$	6,765,766.72

For more detail, refer to the table titled: Surety Estimate Using 2007 Construction Cost Data - Ash Grove Cement Co. - Leamington Plant & Quarry

Surety Estimate Using 2007 Construction Cost Data - Ash Grove Cement Co. - Leamington Plant & Quarry Revised: June 9, 2008 Permit No. MI023/004 costs tom 2007 RSM tear (Costboson Cost Data 21st of softes effective nated

OSP Tot Unit OSP OSP	Cost Description Description Description 1,365.00 Exclavating bulk bank measure, FE Loader, will 1,365.00 Exclavating bulk bank measure, FE Loader, will 1,365.00 Exclavating LOY, no loading 20 c.y dump trainer; 3 1,365.00 Exclavating LOY, no loading 20 c.y dump trainer; 3 1,1156.50 Exclavating LOY, no loading 20 c.y dump trainer; 3 1,1156.50 Exclavating, bulk bank measure, FE loader; with 1,1156.50 Exclavation, bulk bank bank bank bank bank bank bank ban	Cost	88 839.55 Excavaling, bulk bank measure, FE loader, whi mtd, 5 CY cap. C.Y. 3,312.40 Hauling, LCY, no loading, 20 c.y dump trailer, 3 Mt RT. 1,7 lds. C.Y.	Cost	29 941.63 Explosive/molecuse drift no demosal cleet buto.	4		1 800 00 Dump change Miles in that can like soort makes			9,287.34	Cost		22 854 56 Hauling LCV no loading 20 c vidumo tradec 3 MIRT 1744 C V	24	42,385,38		Cost	n'	33	58,455.17	st		
	0.05 Tot. Unit Cost 0.05 0.05 0.05 0.05 0.05 0.05 0.05 0.0	Tot Unit	79 3.92	SRP Tot. Unit Cost	06 0.29					12 1.32		Tot. Unit						P Tot Unit Cost				P Tot. Unit Cost	65 5,85	
			Ш	H			Ш	1	П	120 0		~		Н	Н		-	-				0		

Note									
Unit	× 0 × 2	>0	× 0	× C	Siday		× 0	>0	
Description	093.75 Excavate trench, concrete curb 6-10' does 3/4 CY had back?	Excavating bulk bank measure FE loader whi mid 5 CY ca	94.08 Hauling, LCY, no loading, 20 c.v dumo trailer, 3 MI RT 17 lds, C. v.	432.90 Bacidii structural 200 H.P. 50 haul common earth	23.00 Cutting PVC septic lines with a critical saw	180,00 Dump charges, Moicel urben city fees only bido construration	11.88 Excavating, bulk bank measure. PE loader whi mtd 5 CY can	294.50 Hauting, LCY, no loading, 12 c.y dumo truck, 20 Mi RT, 0.4 lds. C.y.	
Cost	1,093,75	23.76	94.08	432.90	23.00 (180.00	11.88	294.60	1 200
ot. Unit Cost	6.25	0.99	3.92	0.78	4 60	80.00	66.0	24 55	
OSP	1.51	0.19	0.79	0.14			0.19	4.90	40.0
Equip/Mat'is	2.30	0.51	1.07 2.06	0.45	4.60	90.00	0.51	13.60	00.0
Labor	2.44	0.29	107	0.19	Se		0.29	6.05	
CSI Number	3123 1613 0500	3123 1642 1650	3123 2318 1220	3123 2314 4020	0154 3340 6100	0241 1919 0100	3123 1642 165C	3123 2318 0560	2452 5540 47NC
Š	175	24	24	555	2	2	15	12	3.0

	City CSI Number	Labor	Equip/M:	OSP	Tot. Unit	Cost	Description	Note	
8/33 64 25	175 3123 1613 0500	2.44		1.51		1,093,75			
\$3.23.2319 12.C. 100 2.05 0.19 3.82 20.00 Hold beach, including CVT to people, 2001 12.00 CVT to	24 3123 1642 1650	0.29		0.19		23.76			
\$12.23.14 4.020	24 3123 2318 1220			0.79		94.08			
1.00 1.00	555 3123 2314 4020					432.90			
180.00 Unit of June 180.00 Unit of June 180.00 Unit of June Unit of	5 0154 3340 6100		4.60		4 60	23.00			
1.88 Exception CV 1.89 Cot 1.89 Cot 1.89 Cot 1.89 Cot	2 0241 1919 0100				80.00	180.00			
132 3318 3056 6.05 13 50 4.95 24.55 2358 60 18 Juny 12 C.y Currio Ind. 20 VI 1.20	12 3123 1642 1650	0.29		0.19		11,88			
132, 3218 470C 120 0 12 1.32 2.186 Highwain hallings beyond 20 miles, get leasted mile, minimum Mile 1.100 1.100	12 3123 2318 0560	6.05		4.90		294.60			
CSI Number Labor EquipMatts OSP Tot Unit Cost	24 3123 23 18 4700		1.20	0.12		31,58			
2013 2014 dttp: Labor EquipMatta Cat Cost Cost Cost Cat	4 Man Tunnel					2,185,65	197		
3123 2914 400C 0.19 0.14 0.79 2.95 60 Backfill shortural, 200 HP, 50 had common earth CY	Oty CSI Number	Labor	EquipMA	089	Tot. Unit Cost	Cost		Note	
10241 1515 010C 0.13 0.06 0.29 2,085 00 Exploitsive/implicative dnil, no disposal, concluding OFF cost No. 17 10 00C 0.13 0.06 0.29 2,085 00 Exploitsive/implicative dnil, no disposal, concluding OFF Cost No. 17 10 00C 0.13 0.66 0.72 0.50 0.73 0.50 0.74	320 3123 2314 4020	0.19		0.14		249.60		2000	
CSI Number Labor EquipMatts OSP Tot Unit Cost Cost Description Description Unit CSI Number Labor EquipMatts OSP Tot Unit Cost Cost CSI Number	7,100 0241 1615 0100	0,10		90'0		2,059.00			
CSN Number Labor CquipMartis OSP Tot, Unit Cost	5 Break Room/Rest	troom				2,308.60			
123 141 155 010C 0.10 0.13 0.06 1.75 00 0.22 0.175 00 0.25 00 0.25 0 0.25	Oty CSI Number	Labor		OSP		Cost		Note	
12.21 17.500 8.55 4.50 3.95 15.00 6.90 6.136 6.136 6.137 6.205 6.179 6.137 6.205 6.179 6.139 6.139 6.135 6.130 6.139 6.135 6.130 6	6,000 0241 1615 0100	0.10		90'0		1,740.00			
3122 318 12X 0.29 0.51 0.19 0.99 61.38 Excaveling, build park measure, FE loader, with med 5 CY cap C.Y. 3122 318 12X 2.06 0.79 3.82 2.43.04 4.00 C.Y. 3122 318 12X 2.09 1.51 1.65 5.85 2.340.05 Guting, building interior, including disposal, commercial bidg. SF Fir. O241 1927 100C 2.69 1.51 1.65 5.85 2.340.00 Guting, band burning, archaling deposal, commercial bidg. SF Fir. CSI Number 1.20 0.99 1.21 3.65 Selected cutting, band burning, archaling peep, seet to 1/2* filed. LF 5122 2318 003C 0.29 0.51 1.21 3.65 Selected cutting, band burning, archaling peep, seet to 1/2* filed. LF 5122 2318 003C 1.39 0.59 1.51 1.65 3.85 3.65 Selected cutting, band burning, archaling peep, seet to 1/2* filed. CY CY<	44 0241 1317 530C	6.55		3.95		860.00			
23.23.38 12.X 1.07 2.06 0.79 3.92 2.33.04 2.34.00 Guiting, building treater, including dispose, commercal blog, SF Pt. (2.44.1 2.30 1.21 1.65 2.34.00 Guiting, building treater, including dispose, commercal blog, SF Pt. (2.44.2 2.30 1.21 1.21 1.21 1.22 3.65 3.64.42 1.05 3.64.42 1.05 3.65 3.64.42 1.05 3.65 3.64.42 1.05 3.65	62 3123 1642 1650	0.29		0.19	TO SEC. 14	81,38			
1921 1007 2.69 1.51 1.65 5.85 5.340,00 Gutting, building interior, including disposal, commercial bidg, SF Pit. CSI Number Labor EquipMat1s OSP Tot. Unit Cost Cost 35.644.2 CSI Number Labor Cost O.39 Tot. Unit Cost Cost 1.27 236.585 Steel culting, hand burning, including prop. steel to 127 thick Li-F S122 2318 0702 0.29 0.51 0.19 0.99 10.29 Excavaling, building interior, including prob. 1/2 florid CY CSI Number Labor EquipMat1s OSP Tot. Unit Cost O.99 10.29 Excavaling, building interior, including prob. 1/2 florid CY CSI Number Labor EquipMat1s OSP Tot. Unit Cost O.99 10.29 See culting, building interior, including int	62 3123 2318 122C	1.07	2.05	0.79		243.04	Hauling, LCY, no loading, 20 cv dump trailer, 3 MI RT, 17 lds, C.Y.		
CSI Number Labor EquipMat's OSP Tot Unit Cost See Cuting, hand buring, including pep, steel to 127 thick LF 3123 1642 1050 0.50 0.54 0.59 10.19 0.59 10.09 0.59	400 0241 1921 100C	2.69	1.51	1.65		2,340.00	Gutting, building interior, including disposal, commercial bidg. SF Fig.		
CSN Wumber Labor EquipMatis OSP Tot. Unit Cost Cost 356.55 Steat cutting, hand burning, including peop, steel to 127 finick LF 3123 1427 1502 0.29 0.51 0.57 1.21 0.59 10.29 Excavating, built bank measure. File bader with mid. 5 CY cap. CY 3123 1427 1502 0.29 0.51 0.51 0.55	6 Switch Gear #1					5,044.42	Totals		
123 1642 1650 0.20 0.54 0.37 1.21 35.55 5.864 Cubing, hand burning, including pep, steel to 1/2" thick. L.F. 3123 1642 1650 0.59 0.59 0.59 10.59 10.038 Eccavaling, building interior, including pep, steel to 1/2" thick. L.F. 3123 1642 1650 1.48 2.30 1.51 1.65 5.85 45	Oty CSI Number	Labor	Equip/Mat'ls	O&P	Tot. Unit Cost	Cost		Note	
3122 318 000C 148 2.30 103 4.81 490 62 Haufing, LCY, no leading, Sc by dump lanck, 1/2 MI RY, 4.1 las C.Y. 3122 318 000C 148 2.30 103 4.81 490 62 Haufing, LCY, no leading, Sc by dump lanck, 1/2 MI RY, 4.1 las C.Y. 312 318 000C 2.69 1.51 165 5.83 9.522 3.64 ming, LCY, no leading, Sc by dump lanck, 1/2 MI RY, 4.1 las C.Y. CSI Number Labor 1.50 1.65 0.96 7ct Unit Cost 1.50 0.54 0.54 0.5	285 0241 1927 0020	0.20	0.64	0.37	1.21	356.95	1		
1.22.2318 0302 1.48 2.30 1.03 4.81 430.62 Hauling, LCY, no leading 6 c.y dump fuck, 1/2 MIRT, 4.1 Usis C.Y. 1.22.2318 0302 1.51 1.65 5.85 9.582.230 Guttrag, building interior, including disposal commercial bidg. SF Pr. 10.530.83 10.50.8	102 3123 1642 165C	0.29		0.19		100.98	Excavating, bulk bank measure, FE loader, whi mtd, 5 CY cap C.Y.		
10241 1902 2.69 1.51 165 5.85 10.350.35	102 3123 2318 0030	1.48		1.03		490.62	Hauling, LCY, no loading, 6 c.y dump lnuck, 1/2 MI RT, 4,1 lds C.Y.		
CSI Number Labor EquipMat'ls OSP Tot Unit Cost Cost Description Description Unit CSI Number Labor EquipMat'ls OSP Tot Unit Cost LP Cost CP CS CS CS CS CS CS CS	1,638 0241 1921 1000	2.69	1,51	165	5.85	9,582,30	Gutting, building interior, including disposal, commercial bidg, SF Fir.		
CES Number Labor Cost	T Electric Sub Stati	no				10,530.85	lotals		
2805 0510 100	Oty CSI Number	Labor	Equip/Mat/15	OSP		1.00		Note	
258 251 251 252 253 254 255	612 0241 1360 170C	1.70	0.55	0.36		1,984.52			
13.00 13.0	6 2805 0510 157C	785.00	149.00	*******	1	8,100.00			
C281 2010 662Z 435 60 48.40 484 00 121 00 Hazardous W clinybuldspt. dumperle disposal change, max Ton 0241 1927 002C 0.20 0.64 0.37 1.21 196.02 1 20 cert building sele.] * Thick plate L.F. 36 No 105 0.50 0.75 20.412.03 Sile dmil. conc. 7* to 25° Thick, plane C.Y. 3123 2318 003C 1.46 2.30 1.63 2.80 3.45 2.80 1.41 los. CY 3123 2318 172C 1.0 0.99 3.45 2.80 Hauling, LCY, no loading, 8 c.y dump buck, 12 M RT, 17 los. CY 3.82 1.317.12 Hauling, LCY, no loading, 20 cy dump buck, 17 los. CY 1 Waste Of Casoline, ## Disesel, & #T Disesel, Storage 3.800.30 1.317.12 Hauling, LCY, no loading, 20 cy dump buck, 17 los. CY 1.10.11 CSI Number Labor Equipment 1.00 loading, 20 cy dump buck, 17 los. CY 1.00 loading, 20 cy dump buck, 17 los. CY	4 0281 2010 311C		118.80	13.20		528.00			
3123 1442 165C 0.20 0.64 0.37 1.21 150.02 Sile drill, control thing sheel 1" thick plate C.Y. 3123 1642 165C 0.29 0.51 0.19 0.99 337.22 Exclavating butk bark measure, FE badler, whi mid. 5 CY cap. C.Y. 3123 2318 0.32 1.45 2.30 1.03 4.61 2.46 1.37.12 Haufing, LCY, no loading, 8 c.y damp track, 12 M.R.T. 4 Hds. C.Y. 3123 2318 172 1.07 3.32 3.32 1.37.12 Haufing, LCY, no loading, 20 cy damp track, 12 M.R.T. 4 Hds. C.Y. 33,000.30 Haufing, LCY, no loading, 20 cy damp tracks, 3 M.R.T. 1 Hds. C.Y. 33,000.30 Haufing, LCY, no loading, 20 cy damp tracks, 3 M.R.T. 1 Hds. C.Y. 33,000.30 Haufing, LCY, no loading, 20 cy damp tracks, 3 M.R.T. 1 Hds. C.Y. 33,000.30 Haufing, LCY, no loading, 20 cy damp tracks, 3 M.R.T. 1 Hds. C.Y. 33,000.30 Haufing, LCY, no loading, 20 cy damp tracks, 3 M.R.T. 1 Hds. C.Y. 33,000.30 Haufing, LCY, no loading, 20 cy damp tracks, 3 M.R.T. 1 Hds. C.Y. 33,000.30 Haufing, LCY, no loading, 20 cy damp tracks, 3 M.R.T. 1 Hds. C.Y. 34,000.30 Haufing, LCY, no loading, 20 cy damp tracks, 3 M.R.T. 1 Hds. C.Y. 35,000.30 Haufing, LCY, no loading, 20 cy damp tracks, 3 M.R.T. 1 Hds. C.Y. 35,000.30 Haufing, LCY, no loading, 20 cy damp tracks, 3 M.R.T. 1 Hds. C.Y.	0 0281 2010 6020	***************************************	435.60	48.40		121.00	П		
See Note 1 60.75 20.412.00 Site drait, conc. 7 to 24 filtide, plan CY. 3123 1642 1803C 0.59 0.59 337.36 Exceeding, C.F. Floads, C.	162 0241 1927 002C	020	0.64	0.37	1.21	196.02			
3122 31462 165C 0.29 0.51 0.19 0.99 337.59 Excavaling, butk bank melsure, FE loader, will mid 5 CY cap C.Y. 3122 2318 003C 1.46 2.30 1.03 4.61 2.80 3.40 3.82 1.317.12 Hauling, LCY, no loading, 8 C.Y. doubt treiler, 3 M.RT. 1.7 His C.Y. 3120 2318 172C 1.07 3.82 1.317.12 Hauling, LCY, no loading, 20 cy dump treiler, 3 M.RT. 1.7 His C.Y. 33,000.30 4.00 20 20 20 20 20 20 20 20 20 20 20 20 2	336 See Note 1					20,412.00			
3122 2318 003C 1.45 2.30 1.03 4.81 2.40 Halling, LCY, no leading, 50 cy dump truck 112 MIRT 4 1 lds. CY. 3123 2319 122C 1.07 2.06 0.79 3.82 1.317.12 Halling, LCY, no leading, 20 cy dump trailer, 3 MIRT 1 lds. CY. 33,000.30 1.317.12 Halling, LCY, no leading, 20 cy dump trailer, 3 MIRT 1 lds. CY. 33,000.30 1.317.12 Halling, LCY, no leading, 20 cy dump trailer, 3 MIRT 1 lds. CY. 33,000.30 1.317.12 Halling, LCY, no leading, 20 cy dump trailer, 3 MIRT 1 lds. CY. 33,000.30 1.317.12 Halling, LCY, no leading, 20 cy dump trailer, 3 MIRT 1 lds. CY. 33,000.30 1.317.12 Halling, LCY, no leading, 20 cy dump trailer, 3 MIRT 1 lds. CY. 33,000.30 1.317.12 Halling, LCY, no leading, 20 cy dump trailer, 3 MIRT 1 lds. CY.	341 3123 1642 1650	0.29	0.51	0.19		337.59			
3123 2318 122C 1.07 2.06 0.79 3.92 1,317.12 Hauking, LCY, no loading, 20 c.y dump trailer, 3 MIRT, 1.7 lids C.Y. 1. Waste Oil, Gasoline, #2 Diesel, & #1 Diesel Storage CSI Number Labor Equipments CSP Tot Unit Cost Cost	5 3123 2318 0030	1.48	2.30	1.03	1000	24.05	4.1 105		
1 Waste Oil, Gasoline, #2 Diesel, & #1 Diesel Storage CSI Number Labor EquipMatts OSP Tot Unit Cost	336 3123 2318 122C	1.07	2.06	0.79		1,317,12	1.7 lds		
CS Number Labor Equipments 0.8P Tet Init Cost Cost	3-21 Waste Oil Ga	soline. #2	Diesel & #1	Diesel	Storage	33,000.30			
	Oty CSI Number	Labor	Equip/Mat/is	ORP	Tot Unit Cost	Cost		Mate	

	Note									
	Unit	Ea.	Gal	₹ Ea.	Ea	Çai,	· Ea	CY	P CY	S CY
	Description	30.00 Removal of ugnd stor tk, 6000gal to 8000gal tank	572.00 Removal of ugnd stortk, dispose of studge off-site, avg		1,620,00 Removal of ugnd stor tk, 9000gal to 12,000gal tank	,144.00 Removal of ugnd stor lk, dispose of sludge off-site, avg	haul to cer	290.00 Site dml, conc. 7" to 24" thick, plain	18.80 Excavating, bulk bank measure, FE loader, whi mid, 5 CY cap	fauling, LCY, no loading, 20 c.y dump trailer, 3 MI RT, 1.7 ld
	Cost	1,830,00 F	572.00 F	1,716.00 F	4,620,00 F	1,144,00 F	4,620,00 F	7,290,00 \$	118.80	470.40
el Storage	P Tot Unit Cost	915.00	5,72	958.00	1,155.00	5.72	1,155.00	60.75	0.99	3.92
liesel S	ORP	*******	0.57	78.00	-	0.57	Name of		0.19	0.79
Diesel, & #1 L	Equip/Mat/1s	259.00	5.15	780.00	1,050.00	5,15	1,050.00		0.51	2.06
oline, #2.	Labor	410.00	90						0.29	107
18 - 21 Waste Oil, Gasoline, #2 Diesel, & #1 Dies	CSI Number	1265 1030 0120	1265 1030 0390	1265 1030 102E	1265 1030 1029	1265 1030 039C	1265 1030 1026	See Note 1	3123 1642 165C	3123 2318 1220
8-21	£	2 (100	2 (4 (200 (4	120	120	120

0.37 1.27 1.32.9.3.2.2.3.2.2.3.2.3.4.4.1.1.3.7.8.9.2.0.3.4.4.3.1.1.3.7.8.9.3.3.3.2.3.3.3.3.3.3.3.3.3.3.3.3.3.3.3	Note	Note	Note	Note	Note	Note	Note
0.37 1.21 1.21 1.21 1.21 1.22 1.22 1.22 1.22 1.22 1.22 1.22 1.22 1.22 1.22 1.22 1.22 1.22 1.23	Lesel cutting, hand burning, including prep, steel to 1/2" thick. Site dml. conc. 7" to 24" black, plan Excavaling, bulk, barn measure. FE loader, whi mid, 5 CV cap Hauling, LCY, no loading, 50 cy dump buck, 1/2 Mi RT, 1/1 bis Hauling, LCY, no loading, 6 cy dump buck, 1/2 Mi RT, 4/1 lds. Totals	Steel cutting, hand burning, including prep, steel to 1/2" Block. Site and, conc., The 2.4" Block Block. Site and, conc., The 2.4" Block Block. Exceptaing, but bank measure. FE loades, wir mid. 5 CV cap. Hauling, LCV. no loading, 20 c.y dump trailier, 3 M RT, 1,7 lds. Hauling, LCV. no loading, 6 c.y dump trailier, 3 M RT, 1,7 lds. Hauling, LCV. no loading, 6 c.y dump block. 1/2 MI RT, 4.7 lds. Cutting, building interior, including disposal, commerce blog.		Description Descr	136.73 Steel cutting, hand burning, including prep, steel to 1/2" thick. L.F. 37.29 Evaluative/Implosive drin, no disposal, steel blog. C.F. C.F. 550.60 Steel cutting, torch cutting, 1" thick. 159.22 Excavaring, bulk bank measure. FE bodder, whi mid, 3 CY cap. C.Y. 5130.0 Cutting up conveyor best invite location stew. Will mid, 3 CY cap. C.Y. 500.00 Cutting up conveyor best with colocular stew. Siday beautifully LCX no locating, 10.5 s.y dump trainer. Ton 10.7 s. 10.7 c.Y. no locating, 10.5 s.y dump trainer. 20 mi RT, 4 k. C.Y. 10.7 c.Y. 10	1/2 MIRT, 41 ids	Steel to 1/2" thick
		Cost		Cost	Cost	Cost 8	Cost
	11111	H	Halalalala	0.19 0.19 0.79	1	2.30 1.03 Equip/Mat'ls O&P To 2.17 0.59	H 1

Note												Note								Note					9		Note					Note						Note						
		185,33 Excavating, bulk bank measure, FE loader, whilmtd, 5 CY cap C,Y	mp trailer, 3 MI RT, 1,7 ids	6,743.25 Site dml, conc, 7 to 24" thick, piain C.Y	435.12 Hauling, LCY, no loading, 20 c.y dump trailer, 3 MI RT, 1.7 Ids C.Y		89.54 Steel cutting, forch cutting, 1" thick	1.29 Excavating, bulk bank measure, FE loader, whi mtd, 5 CY cap C.Y.	6.25 Hauling, LCY, no loading, 6 c.y dump truck, 1/2 MI RT, 4.1 lds, C.Y.	9,512.63		Cost	g prep, steel to 1/2" thick	9.294.75 Site dinl, conc, 7" to 24" thick, plain	398.97 Excavating, bulk bank measure, FE loader, whi mid, 5 CY cap C.Y		34 154 DO Gutting LCY, no loading 6 cy dump truck, 1/2 MLRT, 4,1 (6s. C.Y.)	46,839.73 Totals 104,839.73		\dashv	R 2013 See Color of the Date of the State of	Excavating bulk back measure FE loader will mid 5 CV can	529.20 Hauling, LCY, no loading, 20 c.y dump trailer, 3 Mil RT, 1,7 ids. C.Y.	1.	Gutting, building interior, including disposal, commercial bidg,	41,181,85	Cost Description Unit	5,561,16 Steel cutting hand fruming, including prep, steel to 1/2" thick L.F.	952,38 Excavaling, bulk bank measure, FE loader, whi mid, 5 CY cap C.Y.	4,627.22 Hauting, LCY, no loading, 6 c.y dump truck, 1/2 MI RT, 4.1 kis, C.Y.		Cost Description Unit		0	104.72 Hauling, LCY, no loading, 6 c.y dump truck, 2 Mi RT, 2.6 ids.fn C.Y.	1,370.25 Excavale trench, confitty, no shifdewing, 1-4/0,3/8 CY tractor C.Y.	A,449,54	Cost Description Unit			5 CV cap	1	AOT 65: Hauten 170 an tanding, pavement removal, pt. 4 to 5 thick ov. 7.	401.00 having, col. ha loseing, 20th young taker, 1 MH R1, 2.5 lds. Col.
Car I'm One Cost	67.0	65:0	3.92	60.75	3.92	0.89	1.21	0.99	4.81			O&P Tot. Unit Cost	1.21	60.75	56.0	3.92	585		Total Hall Court	1.04. Unit Cost	80.75	66.0	3.92	4.81	5.85		OSP Tot. Unit Cost	1.21	66.0	4.81		O&P Tot. Unit Cost	121	0.99	7.70	7.25		O&P Tot. Unit Cost	60.75	3.82	660	2,78	288	837
The state of the	1	91.0 15.0	2.06 0.79	-		0.51 0.19			2.30 1.03			Equip/Mat'ls O&P	0.64 0.37	1		2.06 0.79	151 165		EquipMedic Oct	120	1		2.06 0.79		1.51 1.65					2.30 1,03					3,58 1,55	1.62 2.05		Equip/Mat'ls O&P	Ш		051 0.19	1	140 053	2000
0.0	0.00	67.0	307		000	0.29	020	0.29	1.48			-	0.20		0.29	101	269		l shor	10		0.29	1.07	1.48	2.69		-	0.20	0.29	1.48	0	-	0.20	678	7.30	3.58		Labor	,	1.07	0.29	2 2 2	0.73	2 0
A KOR OSA4 SETE OVOY	127 3455 3843 4867	101 201 0100 1010 1010		111 See Note 1	444 9455 4540 4540	111 3123 1042 1050	/4 UZ41 1927 UUA.	1 3123 1642 1650.	1 3123 2318 0030		30 Warehouse			153 See Note 1	403 3123 1642 1650	340 3453 2348 1441.	5.840 0241 1921 1000	24 Waintenance Ch.	Oto CSI Number	-	135 See Note 1	360 3123 1642 165C	135 3123 2318 1220	225 3123 2318 0030	5,110 0241 1921 1000	32 Bag House	Oty CSI Number	4,596 0241 1927 0020	962 3123 1642 1650	704 3 143 4318 UUSE	33 Water Tank	Oty CSI Number	629 0241 1927 0020	14 3123 1642 1656	14 3123 2318 0100	189 3123 1613 0050	0		396 See Note 1	356 3123 2318 1220	547 3123 1642 165C	- RRG 0041 4247 KOK	151 3129 2318 1150	201 0100 0000

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Mater	BOM								Note				A STATE OF THE STA	2000				Note	atou				Note							N STORY	MON					Note							Note			
Description		loader whi mid 5 my can	254.80 Hauling, LCY, no loading, 20 cv dumo trader, 3 MI RT 17 de, C.Y.		200	Chal.	1	Description	-		27.8 98 Hauling LCV no loading 6c vident fruit 1/2 MIRT 4.1 life C.V.	Otals	Deconotion	7.489.82 Explosive/molosive drill no disposal concibido	mtd 5 CY cap		Totals	Description	nrab steel in 1/7" think	6			Description	oreo steet to 10" thick		foading, 6 c.y dump fruck, 1/2 MI RT, 4.1 ids, C.Y.	mp trailer, 3 MI RT, 1,7 lds		Totals	Description	conc blde			14.742.00 Gutting, building interior, including disposal, commercial bidg. SF Fir.	Totals	Description	6,751.80 Steel cutting, hand burning, including prep, steel to 1/2" thick L.F.		p truck, 1/2 MI RT, 4,1 ids.		np trailer, 3 MI RT, 1,7 ids	Totals	Description	9531.17 Steel cutting, hand burning, including prep, steel to 1/2" thick L.F.	ank measure, FE loader, whi mid, 5 CY cap C.Y.	loading, 6 c.y dump truck, 1/2 Mt RT, 4.1 ids. C.Y.
5580	3.948.75 Site dral conc. 7" to 24" thick olain	64 35 Excavation bulk b	254.80 Hauling, LCY, no.	2.310.00 Removal of upnd	572.00 Removal of ugnd	2.310.00 Removal of upnd	9,459.90	Cost	1	67.45 Economics to the	278 98 Hauling LCY no.	474.34	Cost	7.489.82 Explosive/mplosiv	944,46 Excavating, bulk b	3,739.68 Hauling, LCY, no l	12,153,96	Cost		40.59 Excavating bulk h	197.21 Hauling, LCY, no.1	408.62	Cost	2.073.94 Steel cutting, hand	568.26 Excavating, bulk b	1,630.59 Hauling, LCY, no.1	921.20 Hauling, LCY, no i	14,276.25 Site dml, conc, 7" to 24" Ihick, plain	19,470.24	Cost	Г	106.92 Excavating, bulk b	423.36 Hauling, LCY, no i	14,742.00 Gutting, building in	16,117,92	Cost	6,751.80 Steel cutting, hand	1,237.50 Excavating, bulk b	5,247,71 Hauling, LCY, no l	9.659.25 Site dml. conc. 7" to 24" thick, plain	623.28 Hauling, LCY, no l	23,519.54	Cost	9.531.17 Steel cutting, hand	Z 303,73 Excavaing, bulk b	11,192,87 Hauling, LCY, no.
O&P Tot. Unit Cost	- 80.75	0.19 0.99		1.1	0.57 5.72	1,155.00		O&P Tot Unit Cost					OKP Tot Unit Cost	0.06		0.79 3.92		OSP Tot. Unit Cost	0.37 1.21				O&P Tot. Unit Cost	0.37 1.21			0.79 3.92	. 60.75		OSP Tot. Unit Cost :				1.65 5.85		O&P Tot. Unit Cost			1.03 4.81	. 60.75	0.79 3.92		OSP Tot. Unit Cost			1,03
or Equip/Mat'ls		0.29 0.51		1,050.00	- 515	1,050.00		or EquipMatils	10				or Equip/Mat/Is	0.10 0.13		1.07 2.08		or Equip/Mat/1s	0	0.29 0.51			or EquipMails (0.20 0.64		1.48 2.30	1,07 2.06			or Equip/Mat'ls (10			2.69 1.51		or Equip/Mat/is (0.29 0.51	1,48 2.30	١	107 2.06		Equip/M		0.29 0.51	
Oty CSI Number Labor	65 See Note 1			0265 1030 1025	100 0265 1030 0390	2 0265 1030 1025		36 Storage Buildings Oto CSI Number Labor	A 024+1627 C02F			17 - 18 Riend Silvs	Oty CSI Number Labor		954 3123 1642 165C 0		39 Lube & Hvd. Oil Storage	Oty CSI Number Labor	2 0241 1927 002C		41 3123 2318 0030	40 Raw Mill	Oty CSI Number Labor	4 0241 1927 002C	3123 1642 1660		3123 2318 1220	235 See Note 1 -	41 Switch Goar #4		6 0241 1515 0100			2,520 0241 1821 1000 2	42 Finish Mill	Oty CSI Number Labor	5,580 0241 1927 0020 0				159 3123 2318 1220 1	43 Preheat Tower	City CSI Number Labor	7,877 0241 1927 002C 0	3123 1642 1650	2.327 3123 2318 0030

Surety Estimate Using 2007 Construction Cost Data - Ash Grove Cement Co. - Leamington Plant & Quarry

Son					Note						Note							Note	olou				Note	2004					Note					Note				Note							Note					
Description		S CY cap	Total to contrat o cy dottle fock, it will be c.y.		0	Explosive/mplosive dml, no disposal, condibidg C.F. Explosive/mplosive dml, no disposal, condibidg C.F.	11760 Haiding CV on badion 20 e vidimo Iralas 24th bit 47 July CV	364 50 Ste dell conc 7-16 24" thek clain	otals		Description	o prep. steel to 1/2" thick	72.90 Site drai, conc. 7" to 24" thick, plan		4.70 Hauling, LCY, no loading, 20 c.y dump trailer, 3 MI RT, 1.7 ids C.Y.	ng, LCY, no loading, S.c.y dump buck, 1/2 MI RT, 4.1 lds. C.Y.	lotals	Description	cutting, hand burning, including prep, steel to 1/2" thick. L.F.	6.93 Excavaing, butk bank measure, FE loader, whi mtd, 5 CY cap C.Y.	ng. LCY, no loading, 6 c.y dump truck, 1/2 Mt RT, 4,1 lds. C.Y.	lotals	Description	3,359.07 Explosive/implosive dmi, no disposal, concibidg C.F.	mi, conc, 7" to 24" thick, piain	100	1818 88 Hausing LCY, no loading, 20 c.y dump trailer, 3 MI RT, 1,7 lds C.Y.	Totals	Description	culting, hand burning, including prep, steel to 1/2" thick L.F.	9.41 Excavating, bulk bank measure, FE loader, whi mid, 5 CY cap. C.Y.	ng, LCY, no loading, 6 c.y dump truck, 1/2 MI RT, 4 1 lds, C.Y.	S S S S S S S S S S S S S S S S S S S	Description Unit	conc. 7" to 24" think plain	15,187,50 Totals		Description		58 500 00 Gutting, building interior, including disposal, commercial bidg. Sif Fir.	525.59 Excavating, bulk bank measure, FE loader, with mid, 5 CY cap. C.Y.	ng, LCY, no loading, 20 c.y dump trailer, 3 MI RT, 1.7 ids, C.Y.	2,709.18 Explosive/implosive dmi, no disposal, concibida C.F.	100815	Description	II, conc bidg	4,070,25 Site dmi, conc. 7 to 24" thick, plain	loader, whi mtd, 5 CY cap	ng, LCY, no loading, 20 c.y dump trailer, 3 MI RT, 1,7 lds C.Y	
Cost	1,315.27 Stee	127.71 Exc	2,063.47		L061	187.92 EXP	117 60 Hau	364 50 Site	699.72		Cost	3.63 Stee	72.90 She	2.18 Exc	4,70 Hau	4.81 Hau	99.77	Cost	ш	6.93 Exc	33.67 Hau	404.81	Cost		2,128,25 Site	459.36 Exc	1,818.88 Hau	1,183.56	Cost	29 CM Shee	9.41 Exc	45.70 HBU	į	Cost	15.187 50 Ste	15,187,50	Company of the Compan	Cost	16,665.00 Site	58,500.00 Gut	225.69 EXC	2,081.52 Hau	2,709.18 EXDI	66,104,00	Cost	540.27 Expl	4,070,25 Site	134.64 Exc.	533,12 Hau	
O&P Tot Unit Cost		0.90		000	TOT. UNIT COST	560		60.75	The state of the s		O&P Tot Unit Cost	121			3.82	4.81		O&P Tot Unit Cost	1.21	0.89	481		O&P Tot. Unit Cost	0.29	60.75	0.98	3.92		Tot. Unit Cost	1.21	0.99	4.81		Tot. Unit Cost	60.75		THE PERSON NAMED IN COLUMN	O&P Tot, Unit Cost	15.00	5.85	860	28.80	0.23		O&P Tot, Unit Cost	0.29	60.75	0.39	3.92	
	0	230 103	1	Equipolitation Oct	-		206 0.79				⊩	0.64 0.37			0	2.30 1.03		Equip/Mat'ls O&P		0.51 0.19	2.30 1.03			0.13 0.06		°	200 002		0	0	0.51 0.19	2.30 1.03		Equip/Marits O&P Tot. Unit Cost			- 1	-	8	1.51 1.65	0.01 0.18	1	1		EquipfMat'ls O&P	0.13 0.06	П	0,51 0,19	2.06 0.79	
Labor	0.20	1.48		Lahor	0.00	0.29	1.07				Labor	0.20		0.29	1.07	1.48		Labor	0.20	0.29	48		Labor	0.10	*	0.29	170	bui		0.20	0.29	148		Labor .				_	6.55	2.69	0.23	100	0.10		Labor	0.10		0.29	107	-
Qty CSI Number	1,087 0241 1927 002t	129 3123 2318 0030		45 Storage	RAR 0241 1816 010C	30 3123 1642 1650	30 3123 2318 122C	8 See Note 1		8	Qty CSI Number	3 0241 1927 0020	1 See Note 1	2 3123 1642 1650	1 3123 2318 1220	1 3123 2318 0030	47 Stack	Qty CSI Number	301 0241 1927 0020	7 3123 1642 1650	3123 2318 0030	48 Coal Silo	City CSi Number	11,583 0241 1615 0100	35 See Note 1	464 3123 1642 1650	464 3163 6318 1264	49 Kiln Scanner Building	Oty CS! Number	24 0241 1927 0020	10 3123 1642 1650	10 3123 2318 0030		Oty CS! Number	250 See Note 1		-	Oty CS! Number	1,111 0241 1347 530X	10,000 0241 1921 100,	E94 3479 7940 4076	0 347 0541 1615 040F	3,542 UZAL 1613 UJU.	52 Switch Gear #7	City CSI Number	1,863 0241 1615 010C	67 See Note 1	136 3123 1642 1650	136 3123 2318 1220	

187 187	Unit Note Note C.F. C.Y. C.Y. C.Y. M.RT, 17,745, C.Y. M.RT, 17,745, C.Y.	Totals	Note Unit Note No		Unit Note Note Unit Note Unit Unit	Unit Note Note Note Note Note C.F. Note C.F. Note C.F. Note C.F. Note Note	Unit Note Note	Unit Note 10.72 Thick LF C.Y. CR C.Y. Totals	to 1/2" this LF Note 10 1/2" this LF 10 1/2" this SCY Cap C.Y
December Cost December De		The state of the s	1,721 83 Steel cuting, hand burn 177.21 Excavating, bulk bank m 180.99 Hauling, LCV, no loading 2,760.03	4.84 Sieel cutting, hand burn. 455.63 Sie feel, conc., 7 in 547 11.86 Excavating, burk bank in 28.40 Hauking, LCY, no loading 27.85 Hauking, LCY, no loading 523.39	320.55. Steel culting, hend burn 972.00. Site dmi, conc., 71 to 24° 54.45. Excensings, Luk Rahr, m 62.72. Healing, LCY, no loading 197.21. Healing, LCY, no loading 1,609.01.	-	1.780.55 Sheel culting, hand burm 395.56 Hauling, LCY, no loading, 2.139.40 Excevaling, bulk bank m 8.195.28 Hauling, LCY, no badding (6.3.17.72 Explosive Implicate drift (6.3.17.73 Explosive Implicate drift (6.3.15.15)	87.12 Steet cuting, hand burn 8.140.50 Stee dml, corc., 7" to 24" 3.95 Excavabing, bulk bank m 19.24 Hauling, LCV, no loading	
100 11 12 13 14 15 15 15 15 15 15 15		Tot. Unit Cost 1.21 0.99 4.81						Tot. Unit Cost 1.21 60.75 0.99 4.81	Tot. Unit Cost 1.21 60.75 0.99
			-	0.51 2.06 2.30	EquipMat's OSP 064 0.37 0.51 0.15 2.06 0.75 2.30 1.05			EquipMat1s O&P 0.54 0.31 0.51	Equip/Matris O&P 0.50

World	Note						Note						Note				No.	MODE				Note					Note				Note					Media	Note				9000							
12.908.00. Ripping, trap rock, medium hard, 300 HP dozer, adverse cond. C.Y. 7. 2908.00.	Description	prep, steel to 1/2" thick.	11.88 Excavating, bulk bank measure, FE loader, whi mid; 5 CY cap. C.Y.		Y, no leading, 6 c.y dump truck, 1/2 MI RT, 4 1 lds. C.Y.	Totals	Description	plosive drif no disposal, conc bidg C.F.	bulk bank measure, FE loader, whi mtd, 5 CY cap C.Y.	7. no loading, 20 c.y dump trailer, 3 MI RT, 1.7 lds C.Y.	9,504,04			1	117.80 Hauling, LCV, no loading, 20 c.y dump trailer, 3 Mi RT, 1.7 ids. C.Y.	rotals	Description	hand burning, including one steel to 10° thick L.F.	15.05 Excavating, bulk bank measure, FE loader, whi mtd, 5 CY cap CY.	Y, no loading, 6 c.y dump truck, 1/2 Mi RT, 4.1 ids. C.Y.	lotais	Description		6.93 Excavating, bulk bank measure, FE loader, whi mid, 5 CY cap. C.Y. 33.67, Haufinn I CY no loaden is 6 vidimo miss 10 MI DY 4.1 M. C.V.	Totals	Desiration	hand burning including great steel to 1/2 thick F	91.08 Excavating, bulk bank measure, FE loader, writ mid, 5 CY cap, C.Y.	f., no loading, 5 c.y dump truck, 1/2 MI RT, 4.1 lds. C.Y.	IORAIS	Description	74173 Steel cutting, hand burning, including prep, steel to 1/2 thick L.F.				Dacrifolion			225.07 Hauling, LCY, no loading, 6 c.y dump truck, 1/2 MI RT, 4.1 lds. C.Y.		Description	313.20 Explosive/implosive dmil no disposal, concibida C.F.	bulk bank messure, FE loader, whi mid, 5 CY cap, C.Y.	219.52 Hauling, LCY, no loading, 20 c.y dump trailer, 3 MI RT, 1.7 ids C.Y.	nc, 7" to 24" thick, plain C.Y.			
12,908.00 Ripping, tra:	Cost	4.84 Steel cutting	11.88 Excavaling.	29.40 Haufing, LC	21.65 Hauling, LC	964,39	Cost	555.93 Explosive/in	70.29 Excavating.	A Kap Kr. Califford Nation	9,504,04		Cost	204.9U EXPOSIVE/III	117.80 Hauling, LC	382.20	Cost	1	15.05 Excavating,	73,11 Hauting, LC	06.126	Cost	364.21 Steel cutting	33.67 Haufine LC	404.81	Coet	An	91.08 Excavating,	442.52 Hauling, LC	1,732,77	Cost	74173 Sleel cutting	1340 64 Haufing I Ch	76.96 Hauling LC	2,513.75	Cost	1	46.53 Excavating.	225.07 Hauling, LC	676.74	Cost		70.29 Excavating.	219.52 Hauling, LC	972.00 Site dml, cor	181 SG Steel cutting	72.15 Hauling, LC	
0.57 4.00	Tot. Unit Cost	121			(8'6)		Tot. Unit		660				&P Tot. Unit Cost		3.00		O&P Tot Unit Cost	1.21	0.99			O&P Tot. Unit Cost	1,21	4.81		CP Tot Unit Cost	121				O&P Tot. Unit Cost	121	285			Tot Unit Cost	037 121	06.0	4.81		Tot Unit Cost						4.81	
2,55 0.67	EquipMat1s O&P Tot. Unit Cost	0.64 0.3	0	0	2.30 1.03		-		0.51 0.19	1	1		Equip/Mat1s 0&P	9	2.06 0.79		-	-	0	230 103		Equip/Martis O&P		2.30 1.03		Labor Found/Mar7s ORP	0	0,51 0.19			Equip/Mat/1s 0&P	0.64 0.37	1	2.30 1.03	1	Fouity/Mat/1s ORP	0.64 0.37	0.51 0.19	2.30 1.03			0.13 0.06		2.06 0.79		0	2.30 1.03	-
0.78	Labor	0.5			1.40				0.29	1	l		Labor		107		Labor	0	0.29	1.48		Labor	0.20	1.48		Labor	020	0.29	1.48		oor	0.20	107	1.48			020		1.48	Marie	- 1	m	0.29	107			1.48	
3,227 3123 1632 1700	64 Water Supply Well Qty CSI Number	8 See Note 1	12 3123 1642 1650	8 3123 2318 1220	201001020201000	65 First Aid Room	Qty CSI Number	917 0241 1615 0100	74 3472 4546 455	470 0241 1921 100C		66 Instrument Shop	Gty CSI Number	30 3123 1642 1650	30 3123 2318 1220	Ctack	y CSI Number	694 0241 1927 0020	15 3123 1642 1650	15 3123 2318 0030	Stack	Chy CSI Number	301 0241 1927 0020	7 3123 2318 0030	- 11.0	Oth CS! Number	991 0241 1927 0020	92 3123 1642 1650	92 3123 2318 0030	Off-Spec Clinker	Oty CSI Number	358 3123 1642 165C	42 3123 2318 122C	16 3123 2318 0030	Olinbor Pleasador	CSI Number	334 0241 1927 0020	47 3123 1642 165C	47 3123 2318 0030	72 Glocal Dies Buildha	y CSi Number	1,080 0241 1615 0100	71 3123 1642 1650	56 3123 2318 1220	18 See Note 1	150 0241 1927 0020	15 3123 2318 0030	The state of the s

Note		Note				Note							Note				Note				Note					aton	array						Note						Note			
20,436,30 Site dmil. conc. 7" to 24" thick, plain C.Y. 44,842,77 Backfill, shurdural, 200 H.P., 60" haud, sand 8 gravel C.Y.	Fotals	Description Dand Burning Including pages stool to 170" thick F	42.27 Excavating bulk bank measure. FE loader, whi mtd, 5 CY cap C.Y.	39 Hauling, LCY, no loading, 6 c.y dump truck, 1/2 MI RT, 4.1 lds, C.Y.	Joseph Jo	Description	SG demo concrete, plain, 8" thick, avg reinforcing S.F.	Ou demo cast in place pie, 14 -18 and bearing	12 Hauling, LCY no loading, 20 cv duno trailer 3 MIRT 17 lds, CV	35.64 Excavating, bulk bank measure, FE loader, whilmild, 5 CY cap. C.Y.	34 Excavating, bulk bank measure, FE loader, whi mid, 5 CY cap C.Y	10tais			249.48 EXCEVERING, Dulk bank measure, FE loade, whi mid, 5 CY cap. C.Y. 1212.12. Hauling, L.C.Y. no loading, 6 c.y dump truck, 1/2 MI RT, 4.1 lds, C.Y.	of lotals	Description	1.088.43 Steel cutting, hard burning, including prep, steel to 1/2" thick L.F.	C. Excevanting, but bank measure, he loader, will mio, 5 CY cap. C.Y. 39 Hauland, I.C.Y no loading, 5 CY dump truck, 1/2 MIRT, 4.1 like, C.Y.	19 Totals	Description	54 Explosive/mplosive dml, no disposal, concibidg C.F.	75 Site dml, conc. 7" to 24" thick, plain	17 Hauling, off twy haulers, 60 CY rearbot dump, 1000' RT, 3.61 C.Y.	2.527.20 Gutting, building interior, including disposal, commercial bidg. SF Fir. 3,147.25	Description		48 Explosive/implosive dml, no disposal, conc bidg C.F.	32 Excavating, bulk bank measure, FE toader, whi mtd, 5 CY cap C.Y.		2.598.52 Hauting LCY, no loading, 20 c.y dump trailer, 3 MI RT, 1,7 lds C.Y.			Explosive/implosive dml, no disposal, conc bidg	850.50 Site dml, conc, 7" to 24" thick, plan	52 Excavating, bulk bank measure, FE loader, whi mid, 5 CY cap C.Y.	Guiling, building Interior, including disposal, commercial	Totals Totals		2.42. Steel cutting, hand burning, including prep, steel to 1/2" thick. I. F. 3.56. Excavating but bank massure. FE loader whimly 4.09 can. C.y.	20 Ske drui, conc. 7- to 24" thick, pian C.Y.	
20,436.30	65,279.0	1,068	42	205.	1,516.01	Cost	21,316	1 152	141	35.6	56	23,320.85	Cost	2,743.0	1,212		Cost	1,068.43	205	1,316.	Cost	294.64	789.7	85.	3,747.	Cost	252.89	12,183.4	1,552.3	3,027,0	2.598.8	19,661.25	Cost	266 22	850.5	80	2,579.85	3,824,7	Cost	2.6	1.16	63
12 40,29		10t. Unit Cost	0.99	4.81		P Tot. Unit Cost	15.79	1921	3,92	68.0	0.99		Tot. Unit Cost	1,21	4.81		Tot. Unit Cost	121	4 81		O&P Tot. Unit Cost	0.29	90.75	1.67	5.85	O&P Tot. Unit Cost	1.21	0.29	0.99	3,027,00	1.67		P Tot. Unit Cast	0.29	50.75	0.83	5.85		XP Tot. Unit Cost	1.27	60.75	09.6
40.00 0.12		0.37	0.51 0,19	2.30 1.03		Ö	0 0	3.26	2.06 0.79	0.51 0.19	п		OSP	0	2,30 1,03		089	0.54 0.37	-	1	Equip/Mat'ls O&P	0.13 0.06	0.64 0.49	0	1.51 1.65	Equip/Mat/is O&P	-	0	0.19	- 1	0	1	Equip/Mat'ls O&P	0.13 0.08	1	128 029	1.51 1.65		0	0.04 0.37	1	4.61 2.03
0.17		-	0.29	148		-	2 42	16.95	101	0.29	0.29		H	0.20	1,48	To Silos		0.20	1.48		Labor	0.10	0.00	0.17	2.69	Labor	4	0.10	0.29	100	0.17		Labor	0.10	1	0.17	2.69		ы	0.29		2.96
336 See Note 1 1,113 3123 2314 4000	74 Clinker Conveyor	883 0241 1927 002C	43 3123 1642 1650	43 3123 2318 0030	5 Bridge Over Canal	Oty CSI Number	40 00411374 070F	60 0207141400	36 3123 2318 1220	35 3123 1642 1650	6 3123 1642 1650	76 Process Duct	Ohy CSI Number	2.267 0241 1927 002C	252 3123 2318 0030	Cement Dist. Point To Silos	ty CSi Number	43 3123 1642 1650	43 3123 2318 0030	CH year though Chart	Oty CSi Number	1,016 0241 1615 0100	13 See Note 1	51 3123 2318 2130	432 0241 1921 100C	101 Crusher Qty CSI Number	209 0241 1927 0020	012 0241 1615 0100	1,568 3123 1642 1650	1 0154 3360 2780	1,556 3123 2318 2130	102 Lunch Room	Oty CSI Number	918 0241 1615 0100	14 See Note 1	48 3123 2318 2135	441 0241 1921 1000	103 Pump House	Oty CSI Number	4 3123 1642 1650	2 See Note 1	2 3123 2318 0150

Nate					Note							Note						Note						Note								Note				Note					Note							
243.00 Site dril, conc, 7" to 24" bird, 240.00 Site dril, conc, 7" to 24" bird, 240.00 Site dril, conc, 7" to 24" bird, branch concerning Filter and 2 50.00 Site dril, concerning Filter and 2 50.00 Site dril	5.95 Hauling, off twy haulers, 60 CY rearbot dump, 1000 R1, 3,61, C.Y.	95,59 Torch cutting steel. 1" thick plate. 14.00 to 14.00 to 14.00 to 14.00 to 14.00 to 15.00	370.41 Iolais Control Society only during book 5 Mil R1, 2, 1 define Control 370.41	Cost	243.00 Site dral cond. 7" to 24" thick plain	3.90 Excavaling bulk bank measure. FE loader with mid 5.0% cao, C.V.	1,155.00 Removal of ugnd stor tk, 9000gal to 12,000gal tank Es	1,155.00 Removal of ugnd storitk, haul to certified salv dump, 9000gal. Ea.	5.68 Hauling, off hwy haulers, 60 CY rearbot dump, 1000' RT, 3.61 C.Y.	2,563,64	Description	310.97 Steel outling hand burning including piece steel to 1/2" think		27.03 Excavating, bulk bank measure, FE loader, whi mtd, 5 CY cap C.Y.	48.22 Hauting LCT, no loading, 6 c.y dump truck, 2 MI RT, 2.6 ids/h CY.	1,248.94 Totals		Cost Description Oescription Unit	602 50. Site drill conc. 7140 24" the Main.	42.57 Excavating bulk bank measure FF loader whi mid 5 CV can C V	168.56 Hauling, LCY, no loading, 20 cy dump trailer, 3 MI RT, 17 lds, C.Y.	2,340,00 Gutting, building interior, including disposal, commercial bidg. SF Fir.	3,417,60 Totals	Cost Description Unit		388.57 Excavating bulk bank measure, FE loader, will mid, 3 CY cap. C.Y.	23.00 Chould saw rental	790.00 Hauling, LCY, no loading, 16.5 c.y dump trailer, 20 ml RT, .4 k. C.Y	87.12 Highway hauling beyond 20 miles, per loaded mile, minimum, Mile	10,007.41 Totals		Cost de 89 Opes cellura hand burning production coop stand to the table of the	Excavating, hank measure. FE loader will mid 5 CY can		1/4,U3	Cost Description Unit	905.05 Excavating, bulk bank measure, FE loader, whi mid 5 CY cap	7,681.50 Hauling LCY, no loading, 6 c.y dump truck, 2 MI RT, 2 6 lds/h C.Y.	290.40 Steel cutting torch cutting, 1" thick			3.874.42 Steel cutting, torch cutting, 1" thick	1,445.08 Excavating bulk bank measure. FE loader, will mid, 3 CY cap. C.Y.		1390 40 Haufing LCV no loading 165 c volume trafer 20 mi RT 4 ir C V	174.24 Highway hauting beyond 20 miles per loaded mile, minimum Mile	14 400 00 Hardron ICV on loading for dump fairly 4 64 87 2 1 146h, CV	14,400,00 Habiling, Lutt, no taking, o c.y ounp uses, 5 Mi Rt, & 1 learn Lt.
60.75	191	1.21		&P Tot. Unit Cost	60.75	0.99	1,155,00	1,155.00	1.67		ORP Tot Unit Cost	121	60.75	0.59	3.50			O'SE TOT UNIT COST	e0.75	68.0	3.92	5.85		O&P Yot Unit Cost	121	90.00	4.50	15.80	22.0			&P Tot. Unit Cost	68:0	7.70		O&P Tot Unit Cost	0.99	7.70	121		O&P Tot Unit Cost	121	00,00	30.05	15.80	1.32	9 60	25.0
			l	10	1	118	##### C	- N	- 1					0.19	1	1			1	0.19		1.65		1		0.22			203	Ł	1	0		1.68		Н		1.66	1		H		0.22		322	ľ	2.03	
051	128	0.64		Labor Equip/Mat/1s		0.51	1,050.00	1.050.0	1.28		Labor EquipMat7s	0.64	3	0.51	2.06			0.10 cquip/mat is		0.51	2.05	1.51		Equip/Mat1s	0.64	90.00	4.60	8.20	481			Equip/Maris 0 64	0.51	3.68		Equip/Mat1s	0.51	3.68	0.04		Equip/Mat/Is	0 00	00.00	450	8 20	1.20	461	24
0.29	0.17	2.95		Labor		0.29			0.37		Labor	0.20		0.29	101			0.10		0.29	1.07	2.69		$\overline{}$	0.20	0.38		438	208		ł	Cabor 0.20	0.29	2.36		Н	0.29	236	0.20			0.20	0.30		4.38		2.96	25.4
4 See Note 1 6 3123 1642 1650	4 3123 2318 2130	79 0241 1927 002C 2 3123 2318 015C		Oty CSI Number	4 See Note 1	4 3123 1642 1650	1 0265 1030 1025	1 0265 1030 1025	4 312323182130	108 C-111 Cover		12.	12 See Note 1	27 3123 1642 1650	12 3123 2318 1220		S	893 0241 1615 010C	10 See Note 1	43 3123 1642 1650	43 3123 2318 122C	400 0241 1921 100C	108 B-8 Overland Belt	City CSI Number	2.082 0241 1927 0020	29 0241 1819 0100	5 0154 3340 6100	50 3123 22318 1130	377 3123 2318 0150		109 Hopper	123 0241 1927 002C	3 3123 1642 1650	3 3123 2318 0100	110 Transfer Tower	Oty CSI Number	985 3123 1642 1650	240 0244 4827 8050	240 U241 1927 UUCL	Sta	Oty CSI Number	3,202 0241 1927 0020	1,588 5123 1642 1601 40 0241 1919 0107	5 0154 3340 6100	88 3123 2318 1130	132 3123 2318 470C	1 500 3123 2318 0150	1.500 5155 5310 015C

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Cost Reclamation Revegetation of Ultimate Disturbed Area ³
Oty CSI Number Labor EquipMat's O&P Tot Unit Cost

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Totals	30				2,500.00	75,000,00	Spreading composted manure	acre. Reved. pit floor. Blend and spread soil and compos	ed manure
Description						709,621,25			
Cost	Waste Rock Pile Topso	il Redistrib	ution						
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2.30 1.05 3.45 336, 139.00 Mix sole & annel - Fill spread fill, with dozer 300 h p 300 haud 2.30 1.03 4.81 4.81 4.81 4.81 5.81 5.91 5.01 Haufing, LCY, no bading, 6 c. y atmp black, 1/2 MIRT 4 1/65 72.500 00 17.500 00 ber Ameti Soil - Fill spread fill, with dozer 300 h p 300 haud 1,025,690.50 1.02 Ameti Soil - Fill spread fill, with dozer 300 h p 300 haud 1,025,690.50 1.02 Ameti Soil - Fill spread fill, with dozer 300 h p 300 haud 1,025,690.50 1.02 Ameti Soil - Fill spread fill, with dozer 300 h p 300 haud 1,025,690.50 1.02 Ameti Soil - Fill spread fill, with dozer 300 h p 300 haud 1,025,690.50 1.02 Ameti Soil - Fill spread fill, with dozer 300 h p 300 haud 1,025,690.50 1.02 Ameti Soil - Fill spread fill, with dozer 300 h p 300 haud 1,025,690.50 1.02 Ameti Soil - Fill spread fill, with dozer 300 h p 300 haud 1,025,690.50 1.02 Ameti Soil - Fill spread fill with dozer 300 h p 300 haud 1,025,690.50 1.02 Ameti Soil - Fill spread fill with dozer 300 h p 300 haud 1,025,690.50 1.02 Ameti Soil - Fill spread fill with dozer 300 h p 300 haud 1,025,690.50 1.02 Ameti Soil - Fill spread fill with dozer 300 h p 300 haud 1,025,690.50 1.02 Ameti Soil - Fill spread fill with dozer 300 h p 300 haud 1,025,690.50 1.02 Ameti Soil - Fill spread fill with dozer 300 h p 300 haud 1,025,690.50 1.02 Ameti Soil - Fill spread fill with dozer 300 h p 300 haud 1,025,690.50 1.02 Ameti Soil - Fill spread fill with dozer 300 h p 300 haud 1,025,690.50 1.02 Ameti Soil - Fill spread fill with dozer 300 haud 1,025,690.50 1.02 Ameti Soil - Fill spread fill with dozer 300 haud 1,025,690.50 1.02 Ameti Soil - Fill spread fill with dozer 300 haud 1,025,690.50 1.02 Ameti Soil - Fill spread fill with dozer 300 haud 1,025,690.50 1.02 Ameti Soil - Fill spread fill with dozer 300 haud 1,025,690.50 1.02 Ameti Soil - Fill spread fill spr	3,150				18:00	56,700,00	Composted manure (2) 554/cvd soil	ton Resed on a January 2008 set from WRR Industrial	Oreton 18th
2.30 1.03 4.81 467.291.50 Hauding, LCY, no loading, 6 t.y dump truck, 1/2 Mil RT, 4 1 lds 2,500.00 77.5,500.00 Desr. Amdt. Soil - Fill, spread fill, with dozer-300 hp 300 haud 1,025,690.50 Fill spread fill, with dozer-300 hp 300 haud 1,025,690.50 Fill spread fill, with dozer-300 hp 300 haud 10 2,500.00 Fill Soil - Fill, spread fill, with dozer-300 hp 300 hauding, 10 2,500 Fill Soil - Fill, spread fill, with dozer-300 hp 300 Site cleanup 12,00 8,772.00 Site cleanup 12,00 8,772.00 File cleanup 12,00 8,772.00 File cleanup	97,150 3123 2317 019C	0.70	217	0.59	3.46	336,139,00	Mix soil & amdt - Fill, spread fill, with dozer 300 h p 300 hauf		Adam' oran
2,500.00 72,500.00 10.54 Andt Soil - Fill, spread fill, with dozer 300 h p 300 haud quip/Mat/1s O&P Tot Unit Cost Cost Tos 172,00 Sie cleanup 12,00 8,772,00 Sie cleanup 12,00 8	97,150 3123 2318 0030	1.48	2.30	1,03	4.81	467,291,50	Haufing, LCY, no loading, 6 c.y dump truck, 1/2 Mi RT 4.1 lds	C.Y.	
1,025.690.50 Totals Quip/Mat/1s O&P Tot. Unit Cost Cost Description 12.00 8,772.00 Site cleanup Totals	29				2,500.00	72,500,00	Distr. Amdt. Soil - Fill, spread fill, with dozer 300 h p 300 haul	acre. Distribute material on waste rock dumo	
CSI Number Labor EquipMatts O&P Tot Unit Cost Cost Description 12:00 8/772:00 She cleanup Totals	Site Cleanup and Trash	Removal				1,025,690.50	Totals		
8,772.00 Site cleanup 8,772.00 Totals	CSI Number		uip/Mat/ls	O&P Tot	Unit Cost	Cost	Description		
Totals	731				12.00	8,772.00	Site cleanup	acre 1. Assumes 1 laborer @S15/hr can cover 10 acres	er 8 hour shift
						8,772.00			

4,805,888.46	480,588.85	480,588,85	12,810.00	5,779,876,15	965,890.56	6,765,766.72
Subtotal	Contingency (10%) \$	Reclamation Supervision ² (10%) \$	Demob (from attached MOB/DEMOB COSTS FOR RECLAMATION EQUIPMENT \$		Escalate for 5 years at 3.2% per year \$	Rounded Surety Amount in Year 2012 dollars S

9,255,49

Average Cost per Disturbed Acre (731 acres) = \$

Revegelation assumes an area of 497 acres outside the plt, three-quarters of which will be hydrosededs, and one-quarter of which will be seeded via hand broadcasting. It is assumed that composted manure will be applied to one-quarter of this area (124 acres) at an average rate of 5 tons per acre. Also included in this estimate are 30 acres of revegetation inside the pit, all of which will include soil anendments. Seed mix un it costs are based on a January 2008 phone quote from WRR Industries, Ogden, Utah. Seeding (broadcast and hydro) and manure/manure spreading unit costs are based on a January 2008 phone quote from WRR Industries, Ogden, Utah. Notes
All ripping will be performed to a depth of at least 24 inches.
Added Overhead and Profit to tabulation in 2007
Added Overhead and Profit to tabulation in 2007
Concrete demolition unit cost based on a January 2008 phone quote from Strong Brothers Trucking, South Jordan, UTConcrete demolition unit cost based on a January 2008 phone quote from Strong Brothers Trucking, South Jordan, UTConcrete demolition unit cost based on a January 2008 phone quote from Strong Profit and Strong Profit

ASH GROVE CEMENT COMPANY - LEAMINGTON QUARRY, UTAH MOB/DEMOB COSTS FOR RECLAMATION EQUIPMENT RT Mob/Demob Mob Rate Equipment Type Quantity Distance (\$/mi) Cost (mi) Water Truck \$3.50 1 140 \$490 D8 Dozer 2 \$6.50 140 \$1,820 Backhoe, Track Mtd., 3 cyd bucket Backhoe, Track Mtd., 1.5 cyd bucket 2 \$6.25 140 \$1,750 2 \$4.50 140 \$1,260 Haul Truck, 42 cyd cap. \$4.50 \$3,780 6 140 Front End Loader, 5 cyd cap. 3 \$4.50 140 \$1,890 Crane, 150 ton cap., truck mounted Hydromulcher 140 1 \$8.00 \$1,120 1 \$5.00 140 \$700 \$12,810 TOTAL

 ${\tt Mob/Demob}$ estimates based on August 2007 phone quote from Wheeler Machinery, Lindon, Utah, unless otherwise noted.

No pilot vehicles are required for equipment mobilization.

The mobilization point is Draper, Utah.

Appendix
13

ASH GROVE CEMENT - HANK ALLEN PIT RECLAMATION WATERSHED PEAK FLOWS 100-YEAR, 6-HOUR STORM EVENT

Watershed	Watershed Area (sq. ft.)	Watershed Area (acres)	Hydraulic Length - I (ft)	Avg watershed slope - Y (%)	Duration of stom (hr)	Curve Number (CN)	Potential Max. Retention S (in.)	Lag - L (hr)	i Concentrationi	Peak Flow (cfs)
RWS-1	35,479,128	814.5	10,473	52.2	6	81	2.35	0.28	0.47	328.0
RWS-2	3,636,800	83.5	4,080	23.5	6	77	2.99	0.22	0.37	25.3
RWS-3	724,800	16.6	1,440	30.9	6	80	2.50	0.08	0.13	9.2
RWS-4	10,380,800	238.3	6,960	45.9	6	81	2.35	0.21	0.36	109.1

Notes

Watersheds shown on Reclamation Watershed Map attached

S = (1000/CN) - 10

 $L = [(1^{0.8} (S+1)^{0.7}]/(1900Y^{0.5})$

 $T_c = 1.67L$

Peak flow calculated with SCSHYDRO Program assuming a 2.1", 6 hr. long rainfall event with a SCS Type "b" Storm Distribution

Reclamation Channel	Steepest Slope (ft/ft)	Flattest Slope (fl/ft)	Side Slope (ft/ft)	Channel Depth (ft)	Bottom Width (ft)	Peak Flow Velocity (fps)	Peak Flow Depth (ft)
RC-1	0.072	0.037	5H:1V	2.0	18	12.39	1.35
RC-2	0.056	0.003	5H:1V	1.0	30	3.98	0.49
RC-3	0.020	0.020	3H:1V	1.5	0	3.92	0.88
RC-4	0.087	0.087	5H:1V	1.0	20	8.94	0.54
Swale	0.050	0.050	10H:1V	1.5	5	19.03	1.09

Notes

Flow velocities and depths calculated with Flowmaster 6.0 Program

Peak velocities were assumed to occur at the location of the steepest channel slope, and peak depths were assumed to occur at the location of the flattest channel slope

Calculations assume a Manning's roughness of 0.03 (smooth vegetated channel) for all channels and 0.13 (concrete) for the swale RC-3, RC-4, and the swale will have constant slopes.

POND 7 SUMMARY TABLE

Elevation of Invert (ft msl)	4,900.0
Elevation of Crest (ft msl)	4,921.4
Elevation of Spillway (ft msl)	4,920.4
Length of Spillway (ft)	25
Breadth of Spillway (ft)	15
Calculated Annual Sediment Volume (ft³)(a)	6.6
Stage Corresponding to 60% Sediment Capacity/Cleanout Elevation (ft msl) ^(b)	4,900.1
Peak Stage Corresponding to 10-Year, 24-Hour Precipitation Event (ft msl) ^(c)	4,920.3
Volume of 10-Year, 24-Hour Precipitation Event (ft ³) ^(d)	551,939
Maximum Pond Storage volume (ft ³) ^(b)	558,297
Peak Stage Corresponding to 25-Year, 6-Hour Precipitation Event Initiating when Water Impounded to the Spillway Elevation (4920.4 feet msl) ^(e)	4,921.2
Peak Pond Spillay Outflow During the Above-Mentioned Event (cfs)(c)	56.1
Peak Spillway Flow Velocity During the Above-Mentioned Event (ft/s)(c)	2.35

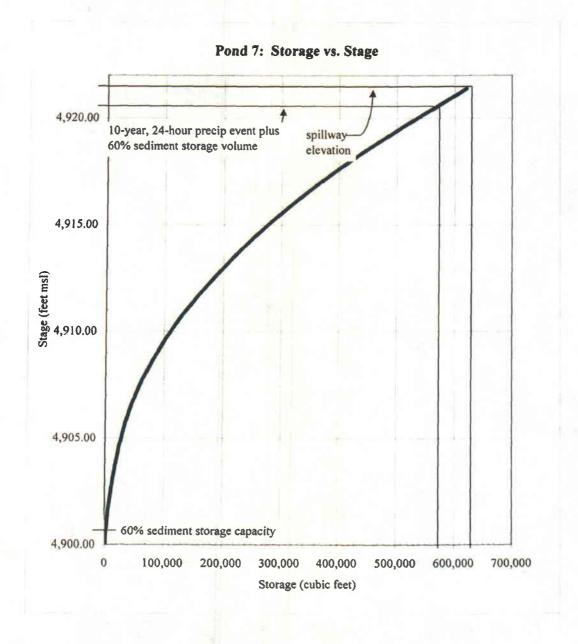
⁽a) Refer to Hank Allen Pit Pond 7 Sediment Yield Calculations Table attached.

⁽b) Refer to Storage vs. Stage graph attached.

⁽c) Refer to Pond 7 10-24 HydroCAD output sheets (p.3) attached

⁽d) Refer to Hank Allen Pit Pond 7 Hydrology Calculations table attached

⁽e) Refer to Pond 7 25-6 HydroCAD output sheets (p.3-4) attached



Runoff Volume

Max. Lag- Concentration Q (in) Volume.	2.82 2.86 4.77 0.37 551,939
Potential Max. the retention S I	78 2.
Watershed Precip. Length - I slope - Y stom (ht) (CN) (CN)	24
Avg watershed slope - Y (%)	0.37
Hydraulic Length - I (ft)	1.78 7,761
Precip. P (in)	
Watershed Arca (acrcs)	415.1
Watershed Area (sq. ft.)	18.083,139
Watershed	POND 7
Storm (Rec. Int Duration)	10-24

Notes

Refer to attached figure for locations of watersheds and soils units

Calculations based on Soil Conservation Service (SCS) Method, National Engineering Handbook Section 4, Chapters 9 & 10 by Victor Mockus, 1972

S = (1000/CN) - 10

 $L = [(1^{0.8} (S+1)^{0.7})/(1900Y^{0.5})]$

 $\Gamma_{\rm c} = 1.67L$

 $Q = (P - 0.2*S)^2 / (P + 0.8*S)$

V = Area * Q

Average Watershed Slope Calculation (Sum of lengths of contour lines X contour interval / Area)

tour	Length
6,750	144
6,550	1,382
6.350	1,856
6,150	3,753
5,950	3,409
5,750	4,902
5,550	992'9
5,350	060'9
5,150	3,278
4,950	1,959
TAL	33,539
Slope	37.1%

Curve Number Calculation

Curve numbers determined using weighted averages of vegetation, disturbance, and NRCS soils areas

(2) CN	603 93	536 76	139	000
). Area (ft.)	2,513,60	15,569,536	18,083,	
Area No.	Dist	Non Dist	TOTAL	A STATE OF N

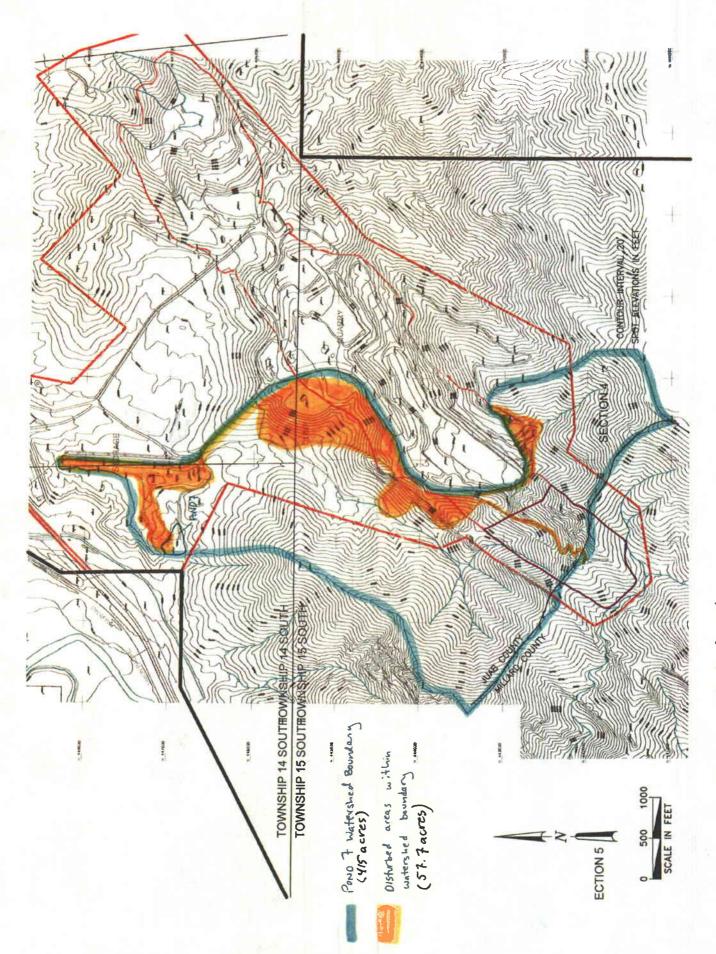
Note: Avg CN = (2 Area, X CN,)/ Total Watershed Area

Curve Numbers for Each Region in Watershed

Hyd Soil Group	٥
Disturbed Areas	93
Non Disturbed	76

Z

The NRCS soils map does not show the hydrologic soil group for all of the soils in the watershed, so they have conservatively been taken as D Curve Numbers for non disturbed areas from UDOT Manual of Instruction Table 7-15 (pinyon-juniper with grass understory, fair (80) to good (71) condition). Curve Number for disturbed areas taken from UDOT Manual of Instruction Table 7-13 (fallow cover with crop residue, poor condition).



Pono 7 watershed and som

HANK ALLEN PIT POND 7 SEDIMENT YIELD CALCULATIONS

A = RKLSVM

Annual Sediment Volume = A X Area / Soil Density

SOUTH PIT

AND DESCRIPTION OF THE PROPERTY OF THE PROPERT		100											Annual
					Slope		Ü					Soil	Sediment
Area				Avg. Slope	Length 1						Α	Density	
No.	Area	Area (ac)	Descr.	S	(ft)	m	LS	R	K	VM	(t/ac/yr)	(pcf)	(ft ³)
1	150,451	3.45	Low Dist'd	9.81%	200	0.5	0.12	7.3	0.05	0.35	0.01	110	
2	127,838	2.93	Low Dist'd	16.98%	200	0.5	0.12	7.3	0.05	0.35	0.02	110	1
3	433,532	9.95	Dist'd	2.81%	150	0.3	0.08	7.3	0.05	0.90	0.03	110	5

TOTAL

L

Notes

Due to the presence of large boulders at the base of the waste rock pile and large undisturbed areas, the portion of the watershed located south of the inlet to Pond #7 was considered to have a negligible sediment contribution. Thus, only the portion of the watershed located north of the inlet (storage area, roads, and disturbed pads and slopes) was considered to contribute sediment to Pond #7.

Refer to locations of areas on attached map.

s = slope angle (%). Taken as the average slope of each area.

l = slope length (ft). This value is defined as the distance from the origin of overland flow to the point of deposition or channelized flow. Slope lengths rarely exceed 400 feet, and in this case, the presence of rocks, trees, and roads, and channels are estimated to limit the slope length to 150 to 200 feet.

m = a factor in the LS equation which is 0.5 for slopes steeper than 5%, and 0.3 for 1-3% slopes .

LS = $((65.41s^2/(s^2+10,000)) + 4.56s/(s^2+10,000)^{0.5} + 0.065) / (1/72.6)^{in}$ (Israelsen et al., 1984)

R is taken from isocrodent map of Utah as 7.3.

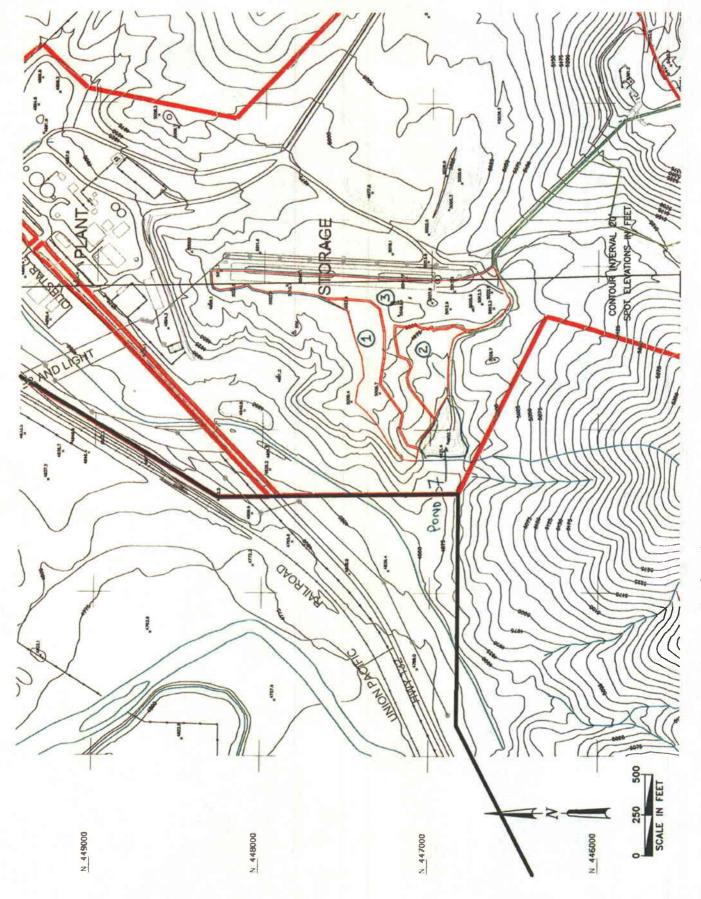
K is taken from NRCS soil surveys as 0.05 (Lodar-Rock Outcrop Complex).

VM values are taken from Table 3 (Isrealson et al, 1984) as follows: 0.35 for undisturbed areas (brush), 0.90 for disturbed areas (bare soil tracked all directions/loose to 12" smooth).

Soil density assumed to be 110 pcf.

Reference:

Israelsen, C. Earl, Joel E. Fletcher, Frank W. Haws, and Eugene K. Israelsen, 1984. Erosion and Sedimentation in Utah: A Guide for Control. Hydraulics and Hydrology Series UWRL/H-84/03. Utah Water Research Laboratory, College of Engineering, Utah State University, Logan, Utah.



Ponp7 Sedinent Yielb Areas

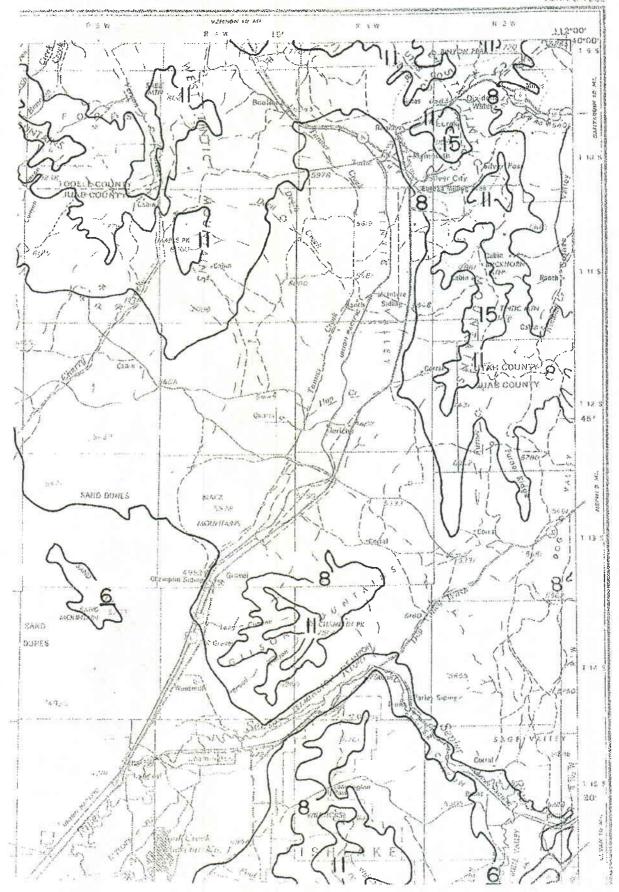


Table 3. Typical VM factor values reported in the literature.a

Condition	VM Factor	Condition	VM Factor
. Bare soil conditions		3. Dust binder	
freshly disked to 6-8 inches	1.00	605 gallons/ac Fiber Glass Rovi	ng 1.05
after one rain	0.89	1210 gallons/acre	0.29-0.7
loose to 12 inches smooth	0.90	4. Other Chemicals	
loose to 12 inches rough	0.80	1000 lb. Fiber Glass Roving	
compacted bulldozer scraped		with 60-150 gallons	
up and down	1.30	asphalt emulsion/acre	0.01-0.0
same except root	.,,,,	Aouatain	0.68
raked	1.20	Aerospray 70, 10 percent cover	0.94
compacted bulldozer scraped	1120	Curasol AE	0.30~0.4
across slope	1,20	Petroset SB	0.40-0.6
same except root	1120	PVA	0.71-0.9
raked across	0.90	Terra Tack	0.66
rough irregular tracked all	0.50	Wood fiber slurry,b 1000	
directions	0.90	lb/acre fresh	0.05-0.7
seed and fertilizer, fresh	0.64	Wood fiber slurry, b 1400	
same after six months	0.54	lb/acre fresh	0.01-0.3
seed, fertilizer, and 12	***	Wood fiber slurry, b 3500	
months chemical	0.38	lb/acre fresh	0.009-0.1
not tilled algae crusted	0.01	Portland Cement and Latex	
tilled algae crusted	0.02	1000 lbs/ac + 8 gal/ac	0.13
compacted fill	1.24-1.71	1500 lbs/ac + 12 gal/ac	0.006
undisturbed except scraped	0.66-1.30	5. Seedings	
scarified only	0.76-1.31	temporary, 0 to 60 days	0.40
sawdust 2 inches deep,		temporary, after 60 days	0.05
disked in	0.61	permanent, 0 to 60 days	0.04
. Asphalt emulsion on bare soil		permanent, 2 to 12 months	0.05
1250 gallons/acre	0.02	permanent, after 12 months	0.01
1210 gallons/acre	0.01-0.019	6. Brush	0.35
605 gallons/acre	0.14-0.57	7. Excelsior blanket with plastic	
302 gallons/acre	0.28-0.60	net	0.04-0.3
151 gallons/acre	0.65-0.70	8. Mulch (see Figures 3, 4, 5, 6)	

aNote the variation in values of VM factors reported by different researchers for the same measures.

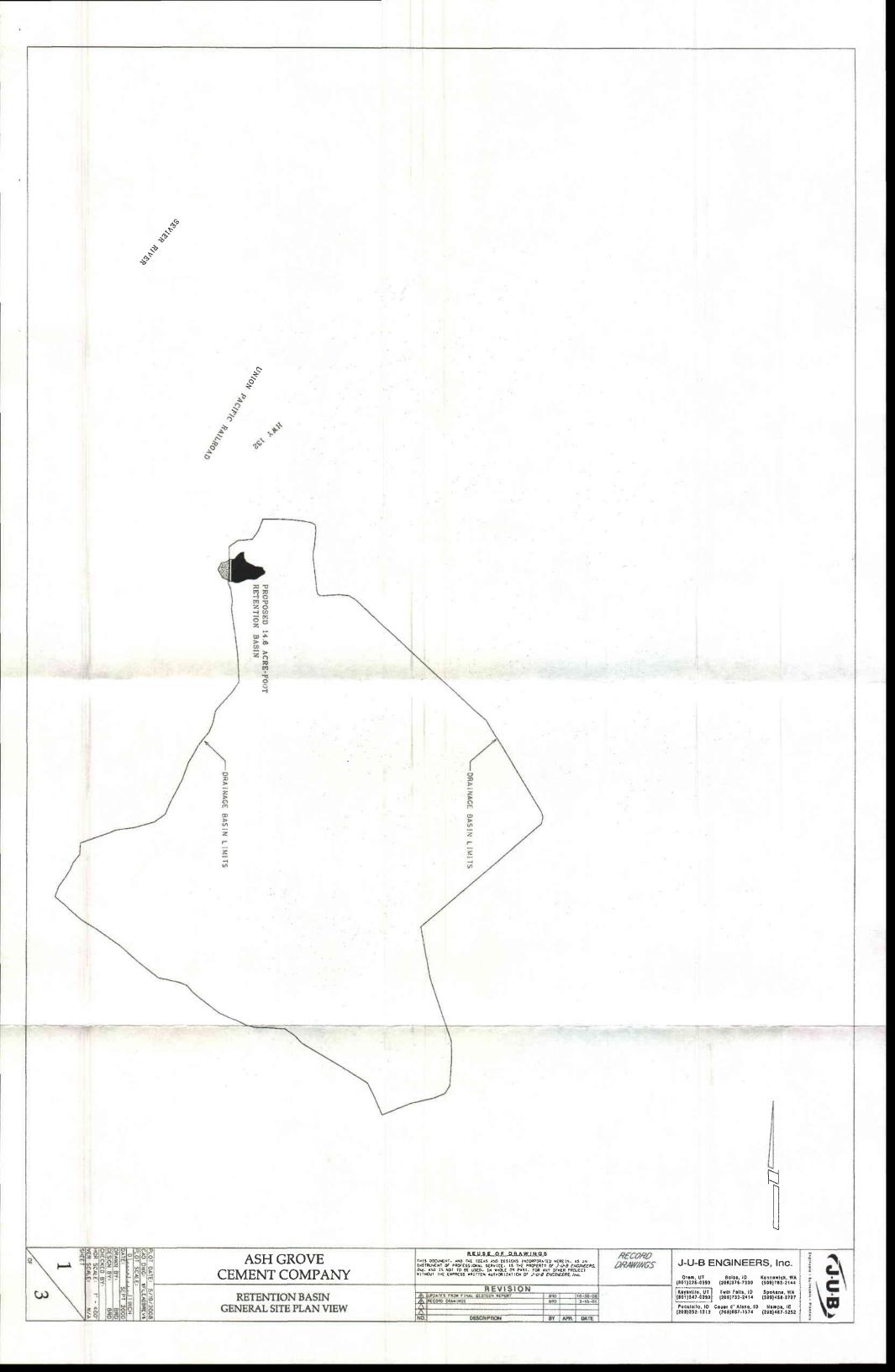
bThis material is commonly referred to as hydromulch.

the critical exposed area will be reduced. A construction operation scheduled in phases is especially valuable in dealing with long slopes, because stabilizing the upper portion of the slope will protect the lower area.

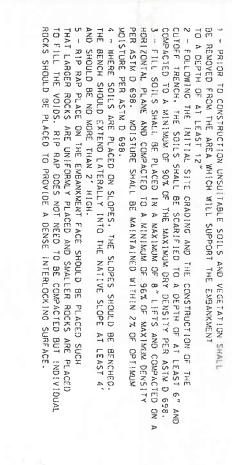
For each phase of construction, control measures which will serve to protect exposed areas and adjacent property, such as sediment traps, basins or ponds, and diversion ditches, should be installed before clearing and grading begin. Structures such as these do not decrease erosion but serve to catch the sediment after it has left the source area. Design drawings for such structures are readily available from local offices of the Soil Conservation Service and from other sources and are not included in this handbook. Even though much research remains to be done in order to determine the true efficiencies

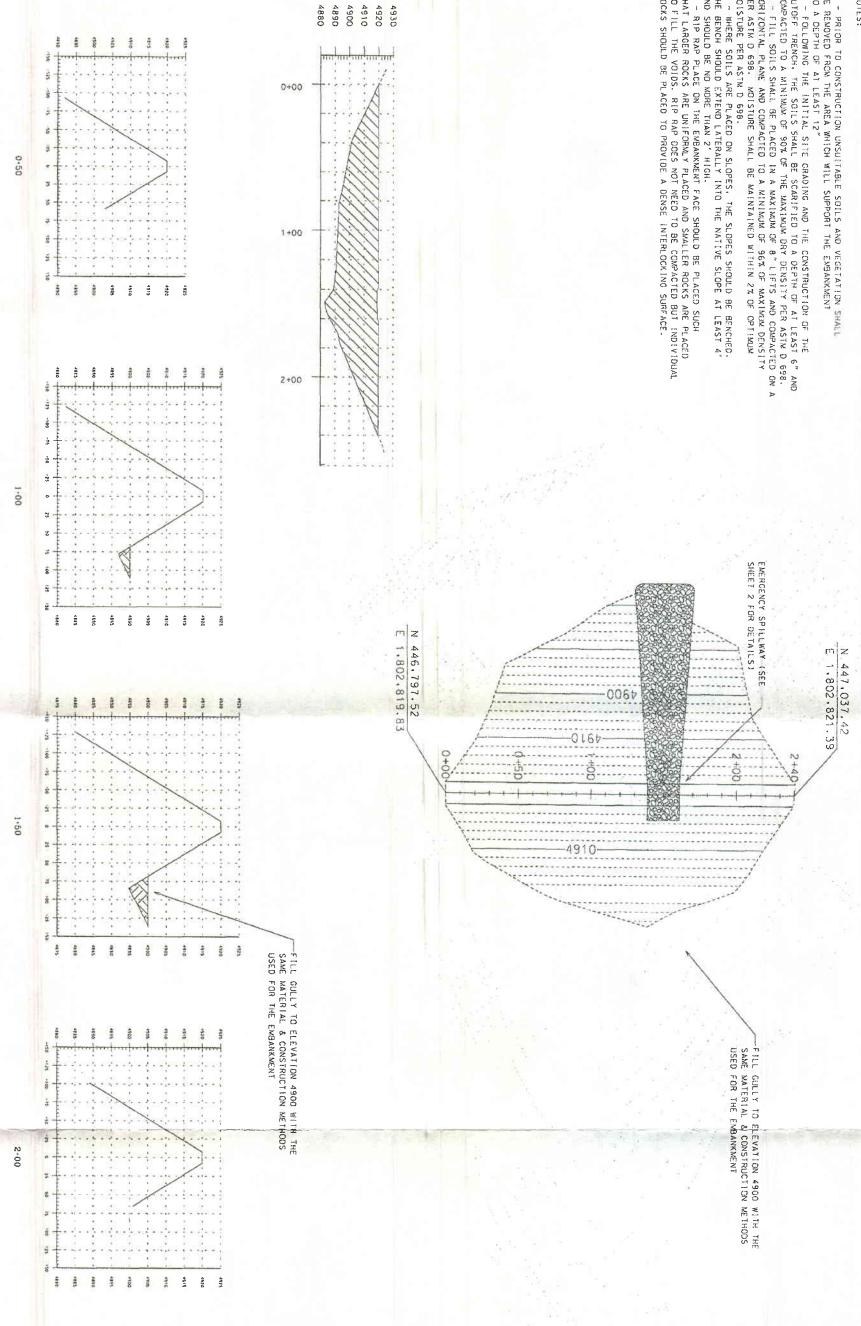
and optimum designs of sediment basins and traps, existing designs may be used effectively to prevent sediment from leaving rights-ofway and entering streams, lakes, or adjacent properties. The amount of sediment captured in such structures can be measured or calculated and subtracted from the total soil loss, determined by the equation, to estimate actual loss. Where areas are to be left for long periods of time, temporary measures such as vegetation, berms, down drains, and mulch covers should be installed to protect and stabilize the exposed soil surface, and then permanent control measures should be implemented as soon as is practical.

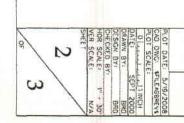
Much can be done to minimize erosion and sedimentation if problems are anticipated and provided for before development begins, and if control measures are implemented in a timely manner.











ASH GROVE CEMENT COMPANY

RETENTION BASIN PLAN VIEW & DETAILS

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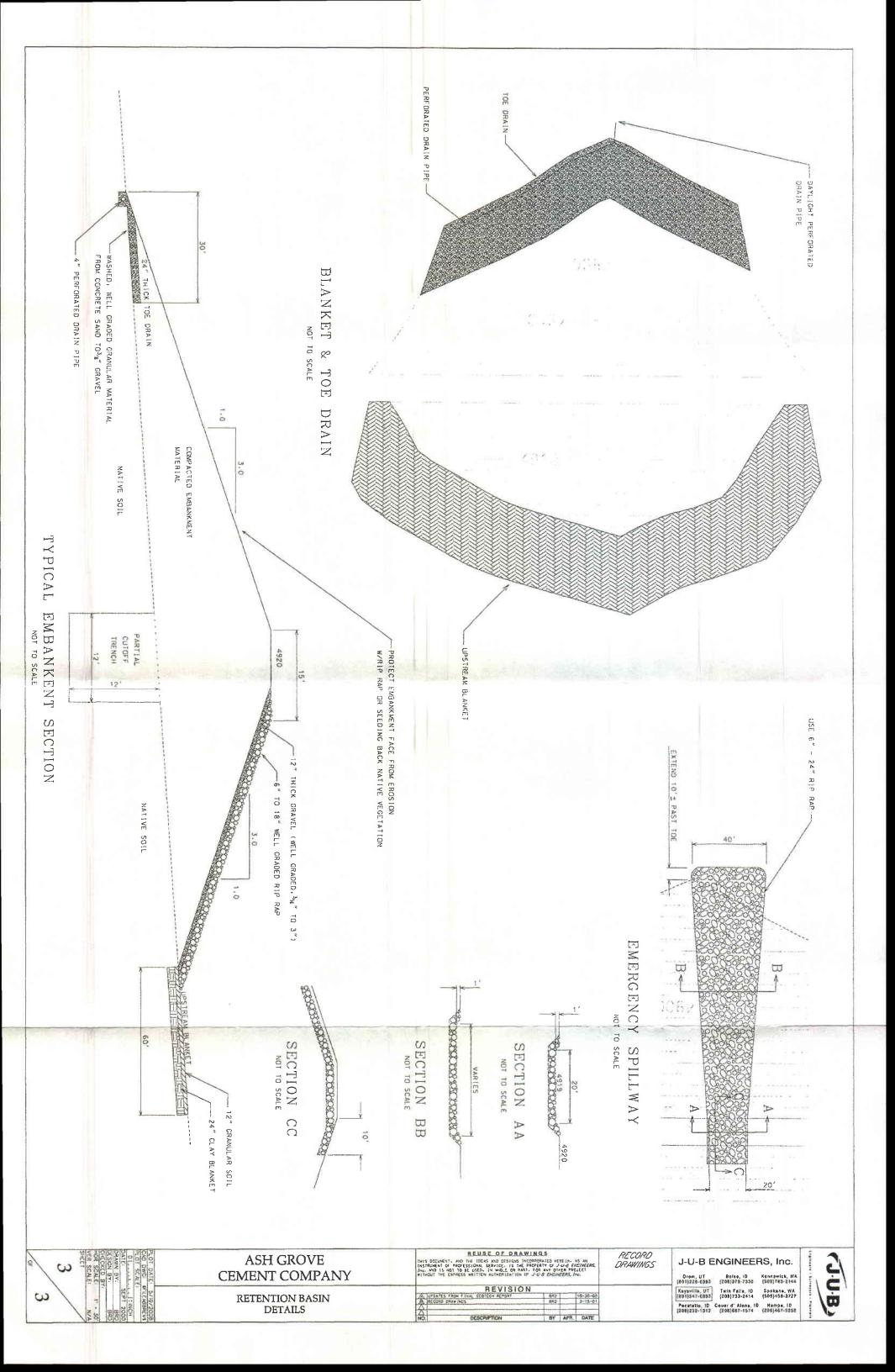
DESCRIPTION

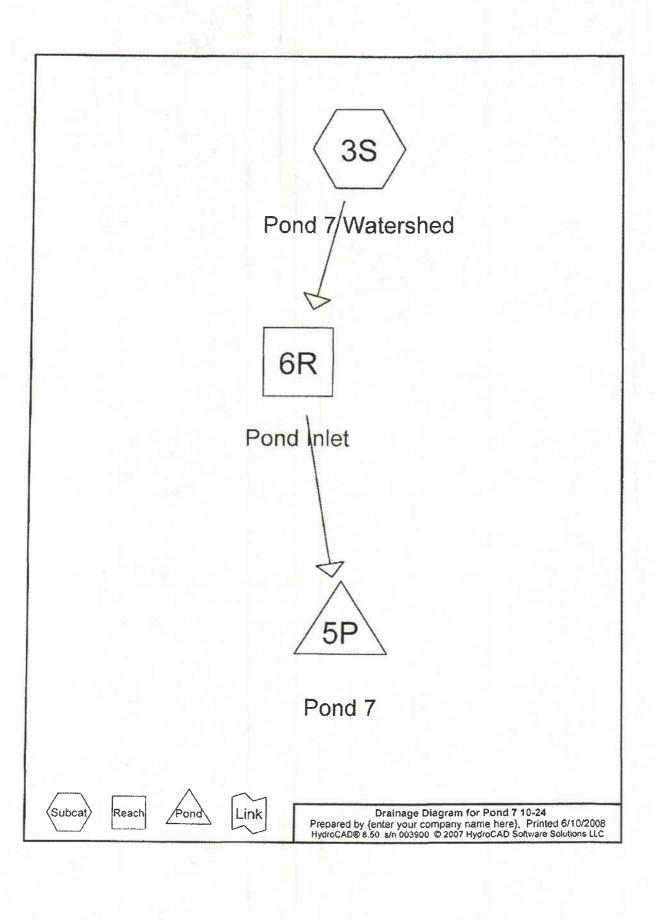
RECORD DRAWINGS

J-U-B ENGINEERS, Inc.

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Pond 7 10-24
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Area Listing (all nodes)

Area (sq-ft)	CN	Description (subcatchment-numbers)		
18,083,139	78	(3S)		
18,083,139		TOTAL AREA		

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Time span=1.00-48.00 hrs, dt=0.01 hrs, 4701 points
Runoff by SCS TR-20 method, UH=SCS
Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment3S: Pond 7 Watershed Runoff Area=18,083,139 sf 0.00% Impervious Runoff Depth=0.37" Flow Length=7,761' Slope=0.3700 '/' Tc=28.6 min CN=78 Runoff=108.50 cfs 551,939 cf

Reach 6R: Pond Inlet

Avg. Depth=0.95' Max Vel=9.56 fps Inflow=108.50 cfs 551,939 cf

n=0.046 L=210.0' S=0.1190'/ Capacity=404.87 cfs Outflow=108.43 cfs 551,939 cf

Pond 5P: Pond 7 Peak Elev=4,920.30' Storage=551,938 cf inflow=108.43 cfs 551,939 cf Outflow=0.00 cfs 0 cf

Total Runoff Area = 18,083,139 sf Runoff Volume = 551,939 cf Average Runoff Depth = 0.37" 100.00% Pervious = 18,083,139 sf 0.00% Impervious = 0 sf

#

Type II 24-hr Rainfall=1.78" Printed 6/10/2008 Page 4

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Summary for Subcatchment 3S: Pond 7 Watershed

Runoff 108.50 cfs @ 12.27 hrs, Volume= 551,939 cf. Depth= 0.37"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 1.00-48.00 hrs, dt= 0.01 hrs Type II 24-hr Rainfall=1.78"

_	A	rea (sf)	CN E	escription		
*	18,0	83,139	78			
	18,0	83,139	F	ervious A	ea	
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
	28.6	7,761	0.3700	4.52		Lag/CN Method,

Summary for Reach 6R: Pond Inlet

Inflow Area = 18,083,139 sf, 0.00% Impervious, Inflow Depth = 0.37"

108.50 cfs @ 12.27 hrs, Volume= 108.43 cfs @ 12.28 hrs, Volume= Inflow = 551,939 cf

Outflow 551,939 cf, Atten= 0%, Lag= 0.7 min

Max. Velocity= 9.56 fps Min. Travel Time= 0.4 min Non-crosive if approved w/ D50=9" Cip Cap

Avg. Velocity = 3.60 fps. Avg. Travel Time= 1.0 min (see HEC No. 11 graph attached) Avg. Velocity = 3.60 fps, Avg. Travel Time= 1.0 min

Peak Storage= 2,381 cf @ 12.28 hrs, Average Depth at Peak Storage= 0.95' Bank-Full Depth= 2.00', Capacity at Bank-Full= 404.87 cfs

> n= 0.0456 (D50 ×5) 0.159 10.00' x 2.00' deep channel, (n= 0.046) Side Slope Z-value= 2.0 '/' Top Width= 18.00' Length= 210.0' Slope= 0.1190 '/' Inlet Invert= 4,946.39', Outlet Invert= 4,921.40'

Doo: avg. rip rap size (in) 5: channel slope (f+/f+) where (Abt et al , 1987) Dso = 9" S=0.1194/44

Summary for Pond 5P: Pond 7

Inflow Area = 18,083,139 sf, 0.00% Impervious, Inflow Depth = 0.37" Inflow 108.43 cfs @ 12.28 hrs, Volume= 551,939 cf

Outflow 0.00 cfs @ 1.00 hrs, Volume= 0 cf, Atten= 100%, Lag= 0.0 min

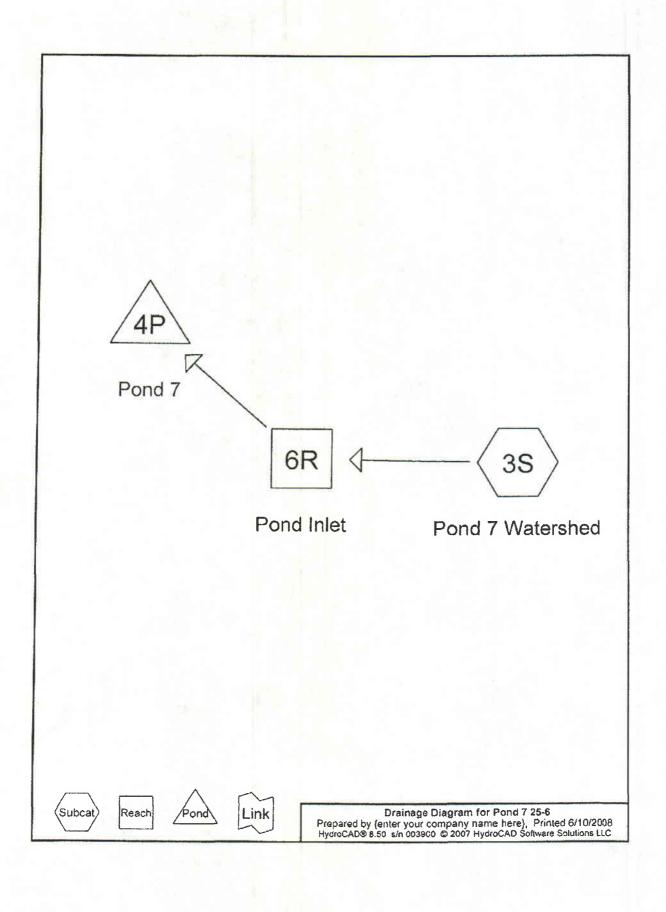
Routing by Stor-Ind method, Time Span= 1.00-48.00 hrs, dt= 0.01 hrs Peak Elev= 4,920.30' @ 26.77 hrs Surf.Area= 61,477 sf Storage= 551,938 cf

Plug-Flow detention time= (not calculated: initial storage excedes outflow) Center-of-Mass det. time= (not calculated: no outflow)

Pond 7 10-24
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Type II 24-hr Rainfall=1.78" Printed 6/10/2008 Page 5

Volume	Invert	Avail.Storag	e Storage	Description	
#1	4,900.00'	620,060	of Custom	Stage Data (Prismatic)	isted below (Recalc)
Elevation (feet)	Surf.A		Inc.Store	Cum.Store (cubic-feet)	
4,900.00	2.0	000	0	0	
4,905.00	•	553	26,633	26.633	
4,910.00	24,6	350	83,258	109,890	
4,915.00	41,	74	166,060	275,950	
4,920.00	61,	336	257,775	533,725	
4,921.40	62,0	000	86,335	620,060	



Pond 7 25-6

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Area Listing (all nodes)

Area	CN	Description
(sq-ft)		(subcatchment-numbers)
18,083,139	78	(3S)

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Page 3

Summary for Subcatchment 3S: Pond 7 Watershed

Runoff 73.32 cfs @ 3.40 hrs, Volume=

300,270 cf, Depth= 0.20"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 1.00-48.00 hrs, dt= 0.01 hrs Type II 24-hr 6.00 hrs Rainfall=1.42"

	Α	rea (sf)	CN E	Description			
٠	18,0	83,139	78		184		
	18,0	83,139	P	Pervious A	еа		
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description	
	28.6	7,761	0.3700	4.52		Lag/CN Method,	

Summary for Reach 6R: Pond Inlet

Inflow Area = 18,083,139 sf, 0.00% Impervious, Inflow Depth = 0.20"

73.32 cfs @ 3.40 hrs, Volume= 73.23 cfs @ 3.42 hrs, Volume= Inflow 300,270 cf

Outflow 300,270 cf, Atten= 0%, Lag= 0.8 min

Routing by Stor-Ind+Trans method, Time Span= 1.00-48.00 hrs, dt= 0.01 hrs

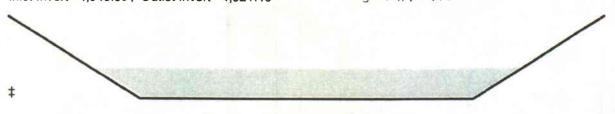
less than max vel. from Max. Velocity=(8.38 fps) Min. Travel Time= 0.4 min This is 10 yr - 24 hr event. Thus, the Avg. Velocity = 4.08 fps, Avg. Travel Time= 0.9 min

loyr - 24 hr event conditions dictate

Peak Storage= 1,835 cf @ 3.41 hrs, Average Depth at Peak Storage= 0.76' rap specs

Bank-Full Depth= 2.00', Capacity at Bank-Full= 404.87 cfs

10.00' x 2.00' deep channel n= 0.046 / n= 0.045 b (050 x 5) 0.159 (Abt, et al., 1981)
Side Slope Z-value= 2.0 '/' Top Width= 18.00'
Length= 210.0' Slope= 0.1190 '/'
Inlet Invert= 4.946 30' Overlet Inv 5 = 0.119 f+/f+ Inlet Invert= 4,946.39', Outlet Invert= 4,921.40'



Summary for Pond 4P: Pond 7

Inflow Area = 18,083,139 sf, 0.00% Impervious, Inflow Depth = 0.20" inflow 73.23 cfs @ 3.42 hrs, Volume= 300,270 cf

Outflow = 56.20 cfs @ 3.61 hrs, Volume= 300,270 cf, Atten= 23%, Lag= 11.6 min

Primary 56.20 cfs @ 3.61 hrs, Volume=

Routing by Stor-Ind method, Time Span= 1.00-48.00 hrs, dt= 0.01 hrs Starting Elev= 4,920.40' Surf.Area= 61,526 sf Storage= 558,297 cf Peak Elev= 4,921.19' @ 3.61 hrs Surf, Area= 61,902 sf Storage= 607,322 cf (49,025 cf above start)

Type II 24-hr 6.00 hrs Rainfall=1.42"

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Page 4

Plug-Flow detention time= (not calculated: initial storage excedes outflow) Center-of-Mass det. time= 19.0 min (273.1 - 254.2)

Volume	ln۱	ert Avail.Sto	rage Storage I	Description	
#1	4,900.	00' 620,0	60 cf Custom	Stage Data (Pr	ismatic)Listed below (Recalc)
Elevatio		Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	
4,900.0	00	2,000	0	0	
4,905.0	00	8,653	26,633	26,633	
4,910.0	00	24,650	83,258	109,890	
4,915.0	00	41,774	166,060	275,950	
4,920.0	0	61,336	257,775	533,725	
4,921.4	10	62,000	86,335	620,060	
Device	Routing	Invert	Outlet Devices		
#1	Primary	4,920.40'	Head (feet) 0.2	20 0.40 0.60 0	0.80 1.00 1.20 1.40 1.60 0 2.64 2.63 2.64 2.64 2.63

Primary OutFlow Max=56.11 cfs @ 3.61 hrs HW=4,921.19' (Free Discharge)
1=Broad-Crested Rectangular Weir (Weir Controls 56.11 cfs @ 2.35 fps)

flow No armor reg'd
on spillway

4.3.1 Estimating Manning's n for Cascading Flow

The average Manning's roughness value, n, was computed for each failure test based on flow velocities and depths measured prior to failure, and are plotted versus the median stone size, D50, in Fig. 4.7. It is observed in Fig. 4.7 that the n values for 1% and 2% slopes fall closely to the solid line representing a relationship developed by Anderson et al. (see Section 4.3.2). However, the n value for each stone size increased as the slope of the embankment increased, and the n value is over 40% higher when Depth/D $_{50}$ < 2 (cascading flow conditions) than when Depth/D $_{50}$ is greater than 2 (Table 4.8).

A median stone size-slope parameter ($D_{50} \times S$) was correlated to the Manning's n value for the CSU data as presented in Fig. 4.8. Combining the median stone size and slope in one parameter appears to have reduced the data scatter. The relationship can be expressed as:

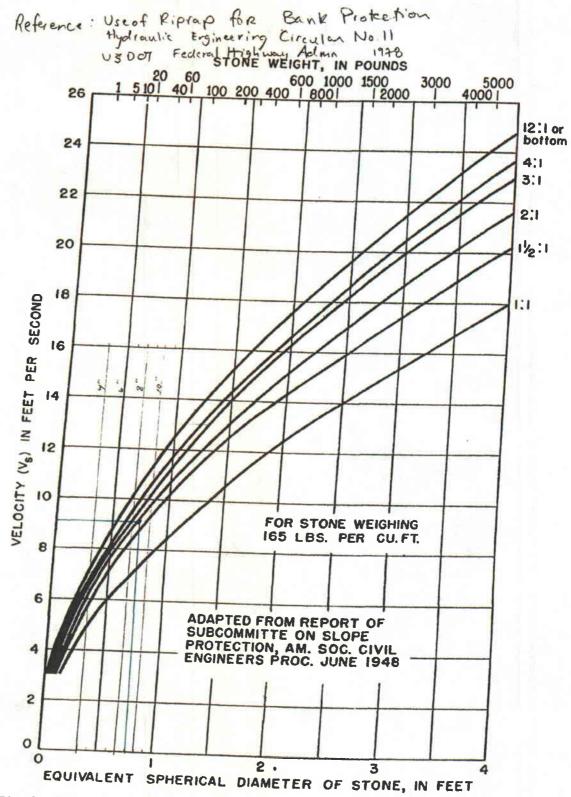
$$n = 0.0456 (0_{50} \times S)^{0.159}$$
 (4.8)

where D₅₀ is in inches. The correlation coefficient, r^2 , is 0.90. Therefore, a Manning's n value can be estimated for a riprapped surface in cascading flow as a function of the median stone size and slope.

4.3.2 Comparison of Procedures

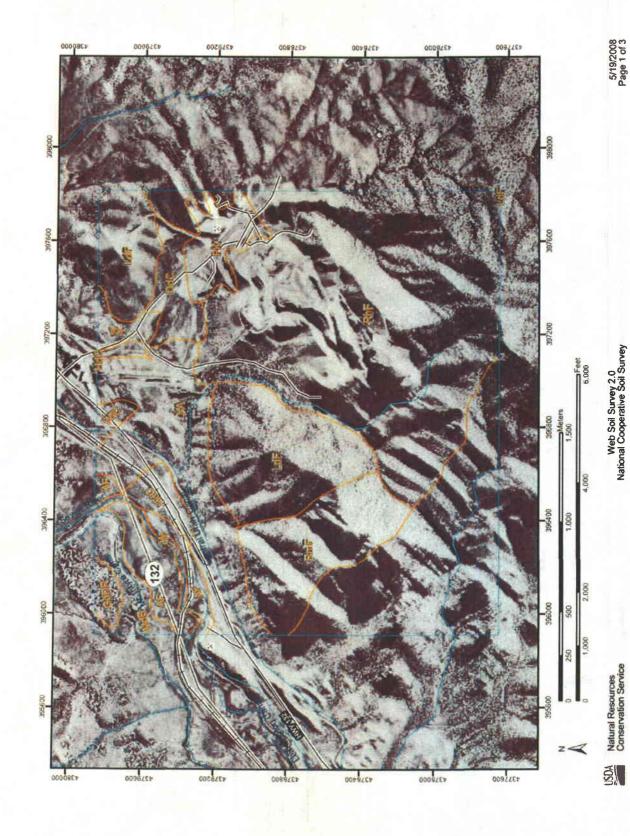
A commonly used expression for determining Manning's n for riprap was presented by Anderson et al. (1970) as

Reference: Development of Riprap Design Critician by Riprap Teshin, in Flumes: Phase 1
SR Abt et al CSU, our page Net 1 Lab USNRC, 1987



FOR VARIOUS VELOCITIES AND SIDE SLOPES

Sill who are



MAP LEGEND

Streams and Canals Interstate Highways Short Steep Slope Very Stony Spot State Highways Special Line Features Local Roads Other Roads US Routes Wet Spot Oceans Other Gully Offher Water Features Transportation 8 : Roads 1 1 ‡ Area of Interest (AOI) Miscellaneous Water Closed Depression Perenmal Water Soil Map Units Mine or Quarry Special Point Features Rock Outcrop Gravelly Spot Sandy Spot Saline Spot Area of Interest (AOI) Borrow Pit Gravel Pit Lava Flow Clay Spot Blowout Landfill Marsh 3 \boxtimes × Soils

MAP INFORMATION

Original soil survey map sheets were prepared at publication scale. Viewing scale and printing scale, however, may vary from the original. Please rely on the bar scale on each map sheet for proper map measurements.

Web Soil Survey URL. http://websoilsurvey.nrcs.usda.gov Source of Map: Natural Resources Conservation Service Coordinate System: UTM Zone 12N This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.

Soil Survey Area: Fairfield-Nephi Area, Utah Version 3, Jan 4, 2007 Survey Area Data:

Division - Parts of Sevier, Millard, Beaver and Piute Counties, Utah Fishlake National Forest - Tushar-Pavant Survey Area Data: Not available Soil Survey Area:

Your area of interest (AOI) includes more than one soil survey area. These survey areas may have been mapped at different scales, with interpretations that do not completely agree across soil survey area a different land use in mind, at different times, or at different levels of detail. This may result in map unit symbols, soil properties, and

Date(s) aerial images were photographed: 8/17/1993; 8/23/1993

magery displayed on these maps. As a result, some minor shifting The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background of map unit boundaries may be evident.

Severely Eroded Spot

Slide or Slip

Sinkhole

Sodic Spot

Stony Spot

Spoil Area

Map Unit Legend

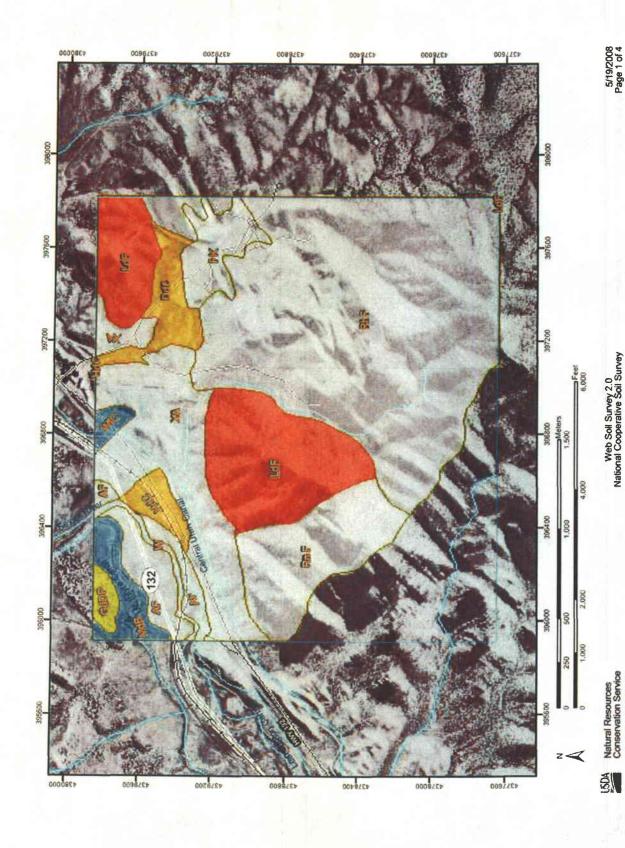
	Fairfield-Nephi Area, U	tah (UT608)	
Map Unit Symbol	Map Unit Name	Acres in AOI	Percent of AOI
AF	Aquic Ustifluvents, saline	52.8	3.9%
DdC	Donnardo stony loam, 2 to 8 percent slopes	38.2	2.8%
GaDP	Goldrun loamy fine sand, hummocky, 0 to 10 percent slopes	10.4	0.8%
HdC	Hiko Peak stony sandy loam, 4 to 8 percent slopes	18.7	1.4%
LdF	Lodar-Rock outcrop complex, 30 to 70 percent slopes	174 1	12.8%
MdB	Manassa-Mellor silt loam, 0 to 2 percent slopes	30,4	2.2%
PK	Pits-Dumps complex	39.5	2.9%
RhF	Rock outcrop-Lodar complex, 30 to 70 percent slopes	515.4	38.0%
RmF	Rock outcrop-Saxby complex, 30 to 70 percent slopes	104.6	7.7%
V	Water	8.4	0.6%
VfC	Woodrow silt loam, 2 to 5 percent slopes	8.3	0.6%
(A	Xerertic Torriorthents, steep	163.7	12.1%

Fishlake National Forest - Tushar-Pavant Division - Parts of Sevier, Millard, Beaver and Plute Counties, Utah (UT649)	
No soil data available for this soil survey area.	

Totals for Area of Interest (AOI)

1,358.2

100.0%



Viewing scale and printing scale, however, may vary from the original. Please rely on the bar scale on each map sheet for proper Original soil survey map sheets were prepared at publication scale. This product is generated from the USDA-NRCS certified data as of Division - Parts of Sevier, Millard, Beaver and Plute Counties, Utah These survey areas may have been mapped at different scales, with of detail. This may result in map unit symbols, soil properties, and interpretations that do not completely agree across soil survey area Date(s) aerial images were photographed: 8/17/1993; 8/23/1993 Your area of interest (AOI) includes more than one soil survey area. a different land use in mind, at different times, or at different levels compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting The orthophoto or other base map on which the soil lines were Fishlake National Forest - Tushar-Pavant Web Soil Survey URL: http://websoilsurvey.nrcs.usda.gov Coordinate System: UTM Zone 12N Source of Map: Natural Resources Conservation Service MAP INFORMATION Soil Survey Area: Fairfield-Nephi Area, Utah Version 3, Jan 4, 2007 of map unit boundaries may be evident. Survey Area Data: Not available the version date(s) listed below. map measurements. Survey Area Data: Soil Survey Area: boundaries. Interstate Highways State Highways Local Roads Other Roads US Routes MAP LEGEND > 1 Not rated or not available Area of interest (AOI) Streams and Canals Soil Map Units Area of Interest (AOI) Oceans Rails 02 05 10 15 Water Features 17 20 24 32 37 43 48 Soil Ratings Transportation Roads ŧ Soils

K Factor, Whole Soil

Map unit symbol	Map unit name	Rating	Acres in AOI	Percent of AOI
AF	Aquic Ustifluvents, saline		52.8	3.9%
DdC	Donnardo stony loam, 2 to 8 percent slopes	.15	38.2	2.8%
GdDP	Goldrun loamy fine sand, hummocky, 0 to 10 percent slopes	.17	10.4	0.8%
HdC	Hiko Peak stony sandy loam, 4 to 8 percent slopes	.15	18.7	1.4%
_dF	Lodar-Rock outcrop complex, 30 to 70 percent slopes	.05	174.1	12.8%
MdB	Manassa-Melfor silt loam, 0 to 2 percent slopes	.43	30.4	2.2%
PK	Pits-Dumps complex		39.5	2.9%
RhF	Rock outcrop-Lodar complex, 30 to 70 percent slopes		515.4	38.0%
tmF	Rock outcrop-Saxby complex, 30 to 70 percent slopes		104.6	7.7%
7	Water		8.4	0.6%
VIC .	Woodrow silt loam, 2 to 5 percent slopes	.43	8.3	0.6%
A	Xerertic Torriorthents,		163.7	12.1%

Description

Erosion factor K indicates the susceptibility of a soil to sheet and rill erosion by water. Factor K is one of six factors used in the Universal Soil Loss Equation (USLE) and the Revised Universal Soil Loss Equation (RUSLE) to predict the average annual rate of soil loss by sheet and rill erosion in tons per acre per year. The estimates are based primarily on percentage of silt, sand, and organic matter and on soil structure and saturated hydraulic conductivity (Ksat). Values of K range from 0.02 to 0.69. Other factors being equal, the higher the value, the more susceptible the soil is to sheet and rill erosion by water.

"Erosion factor Kw (whole soil)" indicates the erodibility of the whole soil. The estimates are modified by the presence of rock fragments.

Rating Options

Aggregation Method: Dominant Condition
Component Percent Cutoff: None Specified

Tie-break Rule: Higher

Layer Options: Surface Layer



POINT PRECIPITATION FREQUENCY ESTIMATES FROM NOAA ATLAS 14



Utah 39.55658 N 112.18827 W 5534 feet

from "Precipitation-Frequency Atlas of the United States" NOAA Atlas 14, Volume 1, Version 4 G.M. Bonnin, D. Martin, B. Lin, T. Parzybok, M. Yekta, and D. Riley NOAA, National Weather Service, Silver Spring, Maryland, 2006

Co	nfide	nce Li	mits		Seas	onalit	y	Loc		xtracted Maps		Other		10	SIS da	ta	Maps	Help	Docs	U.S. Map	,
					Prec	ipita	tion F	requ	iency	Esti	mate	s (inc	hes)								
ARI* (years)	5 min	10 min	15 min	30 min	60 min	120 min	3 hr	6 hr	12 hr	24 hr	48 hr	4 day	7 day	10 day	20 day	30 day	45 day	60 day			
1	0.12	0.18	0.22	0.30	0.37	0.46	0.51	0.66	0.83	1.03	1.16	1.36	1.60	1.81	2.41	2.89	3.62	4.30			
																	4.48				
																	5.40				
												2.41						7.26			
				0.87								2.87		3.71	4.75	5.74	7.03	8.31			
50	0.41	0.63	0.78	1.05	1.29	1.45	1.47	1.62	1.88	2.33	2.68	3.25	3.75	4.14	5.22	6.33	7.71	9.07			
100				1.25		-						3.64		4.58	5.70	6.92	8.39	9.83			
200	0.58	0.89	1.10	1.48	1.84	2.03						4.06						10.55			
500	0.73	1.11	1.38	-	productive many	District Concession of the last of the las	-		OCCUPATION.	CHARLES		Section and district	-	Statement Street, Square, Squa	-	Section 1975	9 92	11 49			

^{*} These precipitation frequency estimates are based on a partial duration series. ARI is the Average Recurrence Interval Please refer to the documentation for more information. NOTE: Formatting forces estimates near zero to appear as zero

	* Upper bound of the 90% confidence interval Precipitation Frequency Estimates (inches)																	
ARI** (years)	5 min	10 min	15 min	30 min	60 min	120 min		6 hr	12 hr	24 hr	48 hr	4 day	7 day	10 day	20 day	30 day	45 day	60 day
1	0.14	0.21	0.26	0.35	0.43	0.52	0.58	0.72	0.90	1.12	1.25	1.48	1.74	1.97	2.60	3,13	3.91	4.66
2	0.17	0.27	0.33	0.44	0.55	0.66	0.73	0.90	1.11	1.39	1.55	1.83	2.16	2.45	3.23	3.89	4.85	5.79
5	0.24	0.37	0.46	0.62	0.76	0.88	0.94	1.12	1.36	1.69	1.90	2.25	2.66	3.00	3.92	4.73	5.85	6.98
10	0.30	0.46	0.57	0.77	0.96	1.07	1.13	1.30	1.56	1.93	2.19	2.62	3.07	3.44	4.45	5.38	6.63	7.88
25	0.40	0.60	0.75	1.01	1.25	1.38	1.42	1.57	1.84	2.27	2.59	3.12	3.64	4.04	5.14	6.25	7.64	9.03
50	0.48	0.73	0.91	1.22	1.51	1.66	1.67	1.80	2.07	2.53	2.92	3.54	4.08	4.51	5.67	6.90	8.39	9.87
100	0.58	0.88	1.09	1.47	1.82	1.98	1.99	2.08	2.31	2.80	3.25	3.98	4.56	4.99	6.20	7.56	9.16	10.70
200	0.69	1.05	1.31	1.76	2.18	2.36	2.39	2.42	2,61	3.08	3.62	4.46	5.05	5.49	6.72	8.22	9.91	11.53
500	0.88	1.34	1.66	2.24	2.77	2.98	3.01	3.03	3.17	3.46	4.12	5.13	5.73	6.18	7.42	9.09	10.91	12.60
1000	1.05	1.60	1.99	2.67	3.31	3.56	3.60	3.63	3.68	3.75	4.52	5.68	6.28	6.72	7.95	9.76	11.68	13.40

1000 | 0.86 | 1.31 | 1.62 | 2.18 | 2.70 | 2.95 | 2.97 | 3.06 | 3.21 | 3.41 | 4.08 | 5.12 | 5.68 | 6.06 | 7.21 | 8.83 | 10.57 | 12.18

Please refer to the documentation for more information. NOTE Formatting prevents estimates near zero to appear as zero

	* Lower bound of the 90% confidence interval Precipitation Frequency Estimates (inches)																	
ARI** (years)	5 min	10 min	15 min	30 min	60 min	120 min	hr	6 hr	12 hr	24 hr	48 hr	4 day	7 day	10 day	20 day	30 day	45 day	60 day
1	0.10	0.16	0.19	0.26	0.32	0.41	0.47	0.60	0.77	0.95	1.07	1.26	1.48	1.67	2.23	2.67	3.34	3.97
2	0.13	0.20	0.25	0.34	0.42	0.52	0.58	0.75	0.94	1.18	1.32	1.55	1.83	2.08	2.76	3.31	4.13	4.92
5	0.18	0.28	0.34	0.47	0.57	0.68	0.75	0.93	1.15	1.44	1.61	1.91	2.25	2.54	3.35	4.00	4.97	5.92
10	0.23	0.34	0.42	0.57	0.71	0.83	0.90	1.08	1.31	1.64	1.85	2.21	2.60	2.91	3.79	4.55	5.61	6.66
25	0.29	0.44	0.54	0.73	0.90	1.04	1.11	1.28	1.53	1.92	2.19	2.62	3.06	3.40	4.37	5.25	6.43	7.60
50	0.34	0.52	0.64	0.86	1.07	1.22	1.28	1.44	1.70	2.13	2.44	2.95	3.42	3.77	4.79	5.77	7.02	8.27
100	0.40	0.61	0.75	1.01	1.25	1.42	1.48	1.62	1.86	2.34	2.70	3.28	3.79	4.14	5.19	6.28	7.61	8.92

^{*} The upper bound of the confidence interval at 90% confidence level is the value which 5% of the simulated quantile values for a given frequency are greater than "These precipitation frequency estimates are based on a partial duration series. ARI is the Average Recurrence Interval.

L	200	0.46	0.70	0.87	1.17	1.45	1.62	1.70	1.84	2.05	2.55	2.97	3.62	4.15	4.51	5.59	6.77 8.17 9.54
																	7.39 8.87 10.30
																	7.84 9.37 10.84

* The lower bound of the confidence interval at 90% confidence level is the value which 5% of the simulated quantile values for a given frequency are less than "These precipitation frequency estimates are based on a period duration mixima series. ARt is the Average Recurrence Interval."

Please refer to the documentation for more information NOTE: Formatting prevents estimates near zero to appear as zero.

Text version of tables

